

تقدم لجنة EiCoM الاكاديمية

تلخيص لمادة:

# الالكترونيات رقمية

للطالبة:

عريب قفيشة

بقلم الطالبة:

قنوت الحيمة

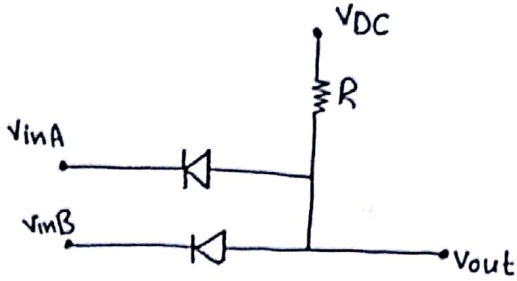


# Digital Electronics

## First 8- "Ch'2' DRL"

DRL cct :

"DRL And gate"  
↓



$$I = \frac{(V_{DC} - V_{\gamma}) - V_{in}}{R}$$

$$-V_{DC} + V_{\gamma} + V_{in} = 0$$

$$V_{in} = V_{DC} - V_{\gamma}$$

\* Diode off :

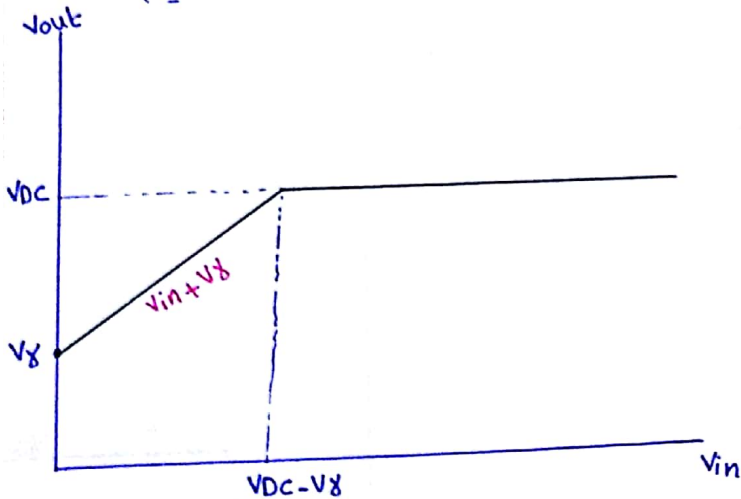
$$V_{in} > V_{DC} - V_{\gamma}$$

$$I = 0$$

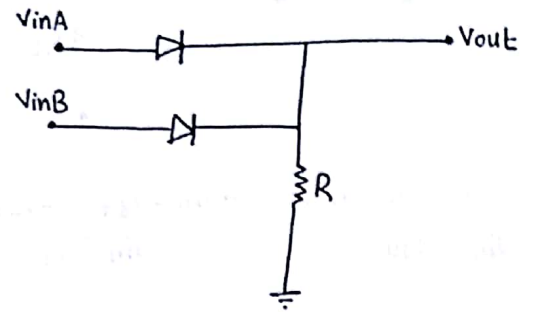
\* Diode on :

$$V_{in} < V_{DC} - V_{\gamma}$$

$$I \rightarrow (\bar{a} \bar{b})$$



\* "DRL OR gate"  
↓



$$-V_{in} + V_{\gamma} + IR = 0$$

$$I = \frac{V_{in} - V_{\gamma}}{R}$$

\* Diode off :

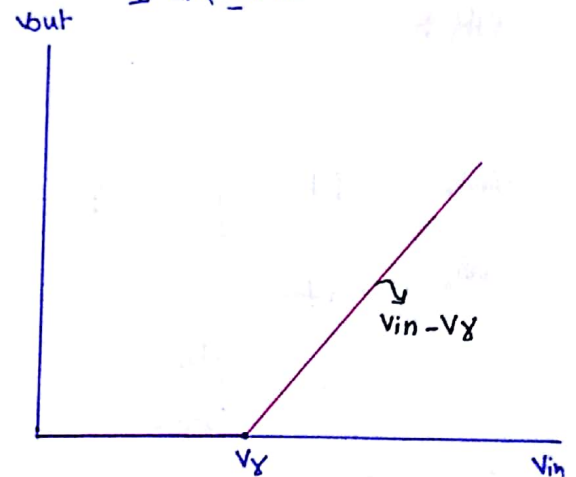
$$V_{in} < V_{\gamma}$$

$$I = 0$$

\* Diode on :

$$V_{in} > V_{\gamma}$$

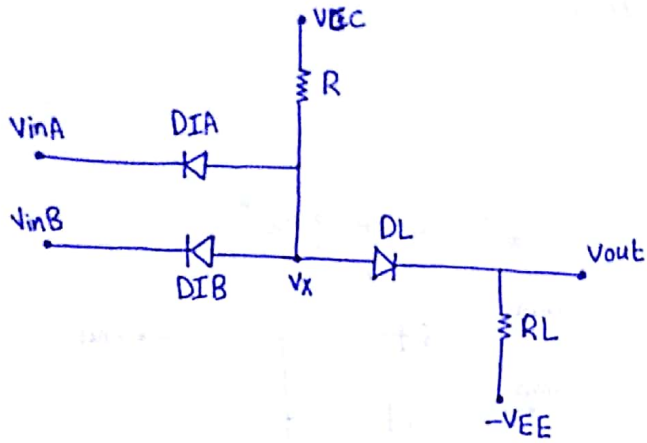
$$I \rightarrow (\bar{a} + \bar{b})$$



$$-V_{out} - V_{\gamma} + V_{in} = 0$$

$$V_{out} = V_{in} - V_{\gamma}$$

**And**

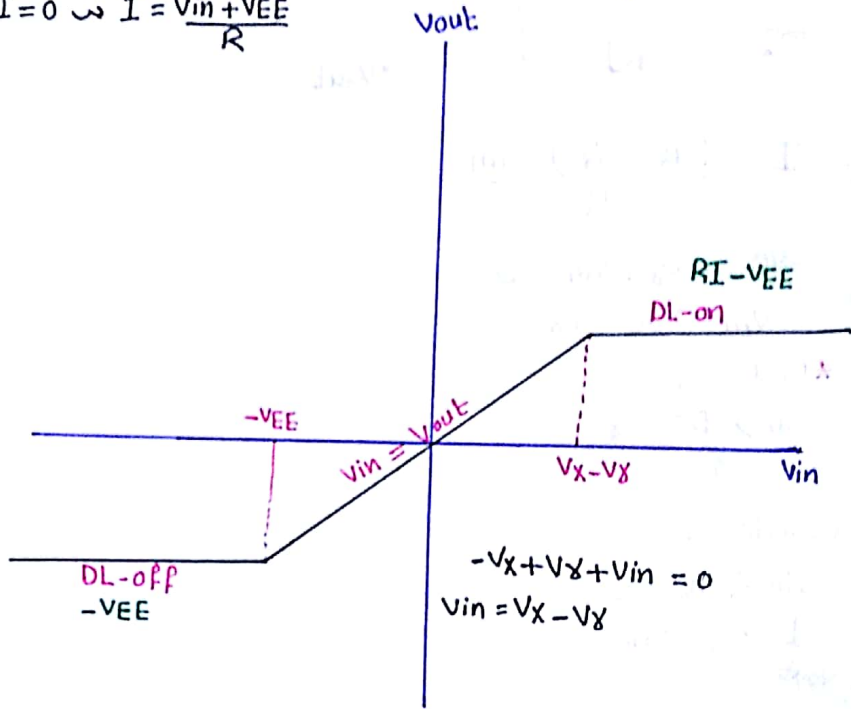


1] DI-on, DL-on :-  $-V_{in} - V_{\gamma} + V_{\gamma} - V_{EE} + RI = 0 \Rightarrow I = \frac{V_{in} + V_{EE}}{R}$   
 $V_{in} = V_{out}$   
 $V_{in} = V_{EE}$

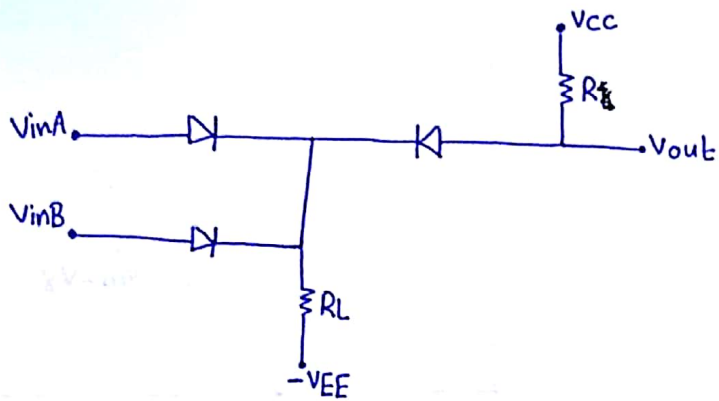
2] DI-on, DL-off :-  
 $V_{out} = -V_{EE}$

3] DI-off, DL-on :-  
 $-V_{CC} + RI + V_{DL} + I R_L - V_{EE} = 0$   
 $I = \frac{V_{CC} + V_{EE} - V_{\gamma}}{R}$

$V_{out} = RI - V_{EE}$



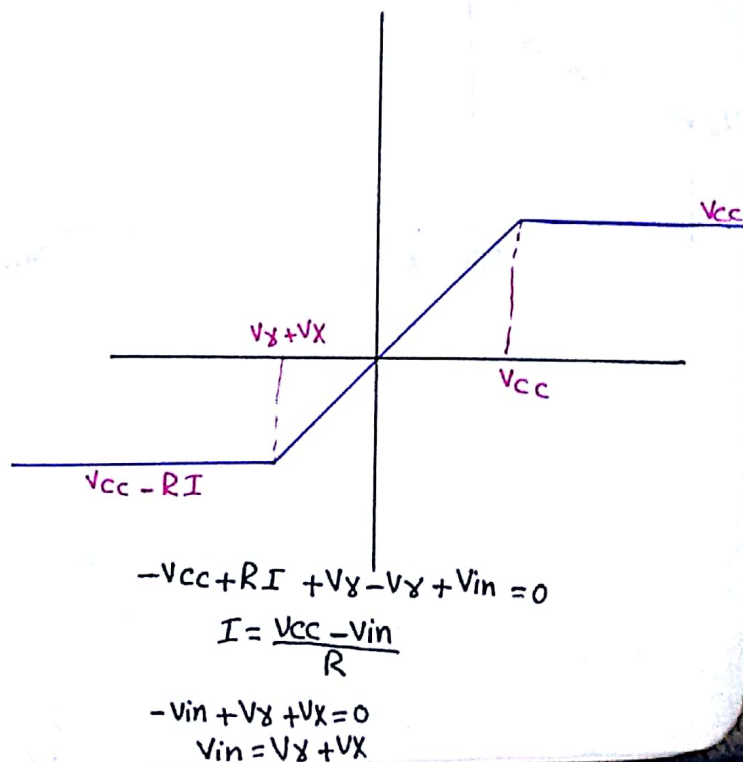
**OR :-**



1] DI-on, DL-on  
 $V_{in} = V_{out}$

2] DI-on, DL-off  
 $V_{out} = V_{CC}$

3] DI-off, DL-on  
 $-V_{CC} + (R+R)I + V_{\gamma} - V_{EE} = 0$   
 $I = \frac{V_{CC} + V_{EE} - V_{\gamma}}{R+R} \Rightarrow V_{out} = V_{CC} - RI$  (2)



$-V_{CC} + RI + V_{\gamma} - V_{\gamma} + V_{in} = 0$   
 $I = \frac{V_{CC} - V_{in}}{R}$

$-V_{in} + V_{\gamma} + V_{\gamma} = 0$   
 $V_{in} = V_{\gamma} + V_{\gamma}$

# Ch "4" :-

## \* Operation modes:

### 1] Cut off

(B-E) ] both  
(B-c) ] reverse

$$I_B = I_C = I_E = 0$$

### 2] F.A

(B-E) FA (B-c) Reverse

$$I_C = \beta I_B$$

$$I_E = (\beta + 1) I_B$$

$$I_E = I_C + I_B$$

### 3] RA

(B-E) RA (B-c) FA

$$I_C = (1 + \beta) I_B$$

$$I_E = \beta I_B$$

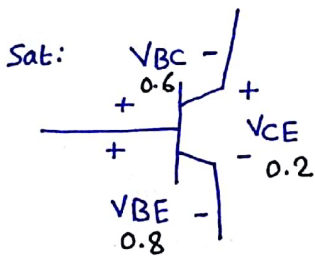
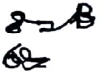
$$V_{BC} (RA) = 0.7$$

### 4] Saturation mode:

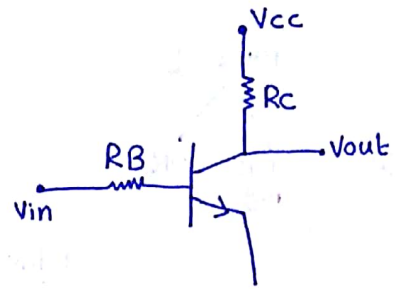
(B-E) FA (B-c) FA

$$I_E = I_C + I_B$$

$$I_E = \beta I_B$$



## \*(TTL)



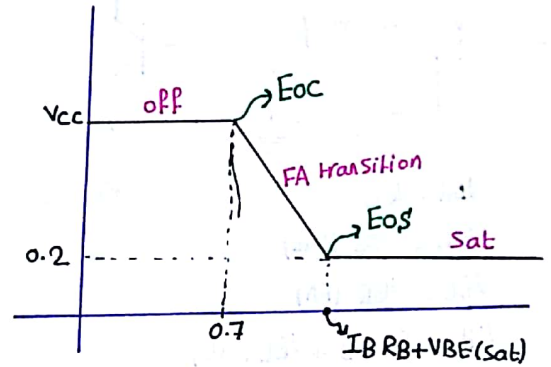
$$V_{OL} = V_{CE(sat)}$$

$$V_{OH} = V_{CC}$$

$$V_{IL} = V_{BE(FA)}$$

$$V_{IH} = I_B R_B + V_{BE(sat)}$$

$$\frac{I_C}{\beta} \rightarrow \frac{V_{CC} - V_{CE(sat)}}{R_C}$$



at  $E_{os} \rightarrow \beta = 1$

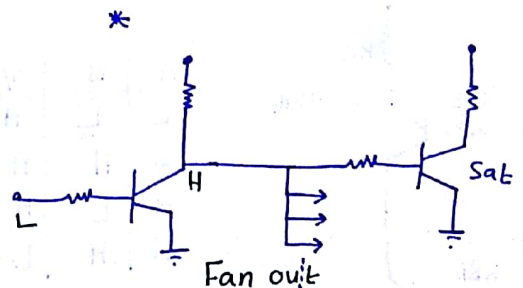
\* pnp  $\bar{v}$   $\bar{v}$   $\bar{v}$  \*

L I/p  $\rightarrow$  Sat

H I/p  $\rightarrow$  off

$$* HNM = V_{OH} - V_{IH}$$

$$LNM = V_{OL} - V_{IL}$$



$$N = \frac{I_{OH}}{I_{IL}}$$

4.2  $\approx$  4  
4.54  $\approx$  4  
4.7  $\approx$  4

دائماً نأخذ integer  
مثلاً!

# Ch "5" RTL

npn

Series



Parallel

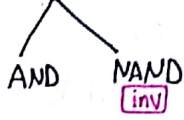


pnp

Series

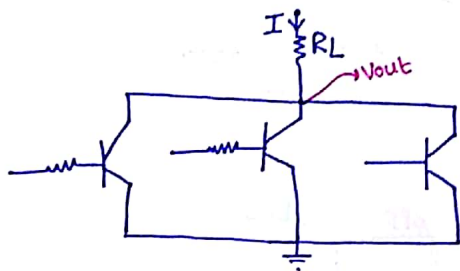


parallel



inv  
C J<sub>1</sub> is o/p J<sub>1</sub> (C-E)

non-inv  
E J<sub>1</sub> is o/p J<sub>1</sub> (C-C)



$V_{OH} = V_{CC}$

$V_{OL} = V_{CE(sat)}$

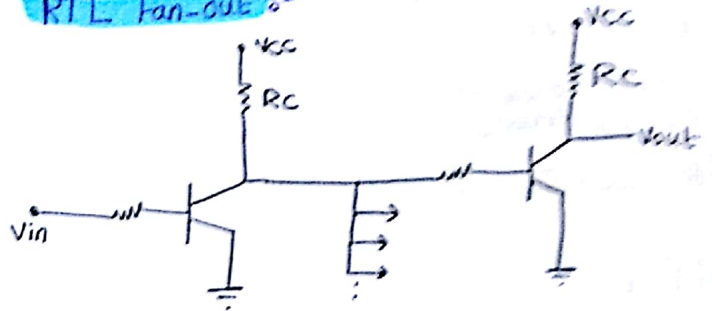
$V_{iL} = V_{BE(FA)}$

$V_{iH} = I_B R_B + V_{BE(sat)}$

A	B	o/p
L	L	H
L	H	L
H	L	L
H	H	L

A+B

## RTL Fan-out :-



$N = \frac{I_{OH}}{I_{IH}}$

$-V_{CC} + I_{OH} R_C + V_{OH} = 0$   
 $I_{OH} = \frac{V_{CC} - V_{OH}}{R_C}$

$-V_{OH} + R_B I_{IH} + V_{BE(sat)} = 0 \Rightarrow I_{IH} = \frac{V_{OH} - V_{BE(sat)}}{R_B}$

$N = \frac{V_{CC} - V_{out}}{V_{out} - V_{BE(sat)}} \cdot \frac{R_B}{R_C}$

$V_{OH} = V_{IH} = I_B R_B + V_{BE(sat)}$   
 $\frac{I_C}{\beta} \rightarrow \frac{V_{CC} - V_{BE(sat)}}{R_C}$

$P_{cc(avg)} = \frac{I_{cc(OH)} + I_{cc(OL)}}{2} \cdot V_{CC}$

$I_{cc(OH)}$  without Load

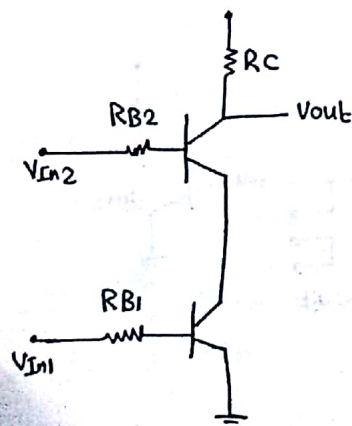
$I_{RC} = I_{CC} = 0$

$I_{cc(OH)} = N I_B = I_{RC} = \frac{V_{CC} - I_{CC} R_C}{V_{out} - V_{BE(sat)}}$

$I_{cc(OH)} = I_{RC} = N \left( \frac{V_{CC} - V_{BE(sat)}}{R_B + N R_C} \right)$

$I_{cc(OL)} = \frac{V_{CC} - V_{CE(sat)}}{R_C}$

## RTL NAND



A	B	o/p
L	L	H
L	H	H
H	L	H
H	H	L

Logic Function =  $\overline{AB}$

$V_{OH} = V_{CC}$

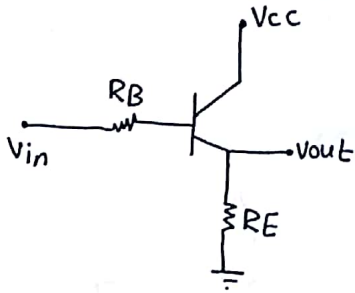
$V_{OL} = N V_{CE(sat)}$  (4)

$V_{iL}$	$V_{iH}$
① $V_{BE(FA)}$	$I_B R_B + V_{BE(sat)}$
② $V_{BE2(FA)} + V_{CE1(sat)}$	$I_{B2} R_{B2} + V_{BE2(sat)} + V_{CE1(sat)}$

(And gate) :-

Sec 5.6:

RTL non-inverter



$V_{OH} = V_{CC} - V_{CE(sat)}$

$V_{OL} = 0$

$V_{iL} = V_{BE(FA)}$

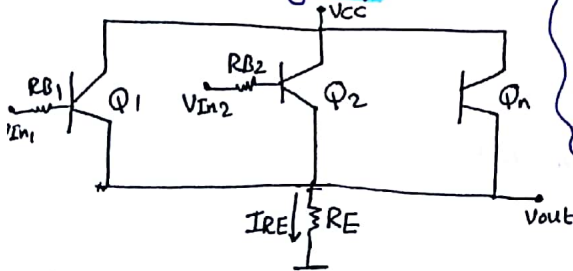
$V_{iH} = I_B R_B + I_E R_E + V_{BE(FA)}$

or  $-V_{iH} + I_B R_B + V_{BC(sat)} + V_{CC} = 0$

$V_{iH} = V_{CC} + V_{BC(sat)} + I_B R_B$

$\frac{V_{CC} - V_{CE(sat)}}{(\beta + 1) R_E}$

non-inv (OR gate)



$V_{OH} = V_{CC} - V_{CE(sat)}$

$V_{OL} = 0$

$V_{iL} = V_{BE(FA)}$

$V_{iH} = V_{CC} + V_{BC(sat)} + I_B R_B$

$\frac{V_{CC} - V_{CE(sat)}}{(\beta + 1) R_E}$

$= I_B R_B + I_E R_E + V_{BE(FA)}$

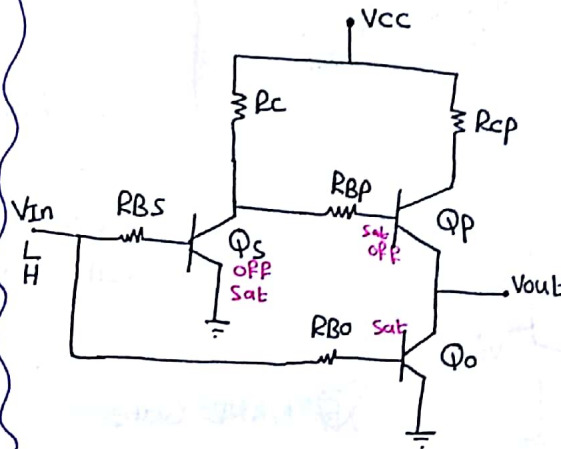
A	B	O/P
L	L	L
L	H	H
H	L	H
H	H	H

$V_{OH} = V_{CC} - N V_{CE(sat)}$

$V_{OL} = 0$

	$V_{iL}$	$V_{iH}$
$Q_1$	$V_{BE(FA)}$	$V_{BE(FA)} + I_B R_B + I_E R_E$
$Q_2$	$V_{BE(FA)} + V_{CE(sat)}$	$V_{BE(sat)} + I_B R_B + I_E R_E + V_{CE(sat)}$

RTL with active pull-up



$Q_O \rightarrow$  pull-down, sink for the load

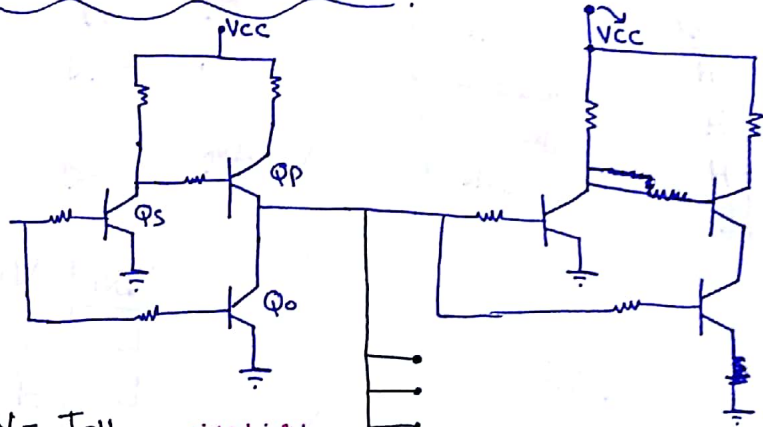
$Q_O, Q_S \rightarrow$  inv

$Q_P \rightarrow$  non-inv

$R_{CP} \approx 0.1 R_C$

$R_{CP} < R_C$

mode  $Q_O, Q_S$    
 mode  $Q_P$



$N = \frac{I_{OH}}{I_{IH}}$    
 *لدينا نقطه 2 لانه التيار متغير بغيره*

$I_{OH} = N I_{IH} = 2N I_B$

$I_{OH} = I_{EP} \approx I_{RCP} = 2N I_B$

$I_{OH} = 2N I_B$

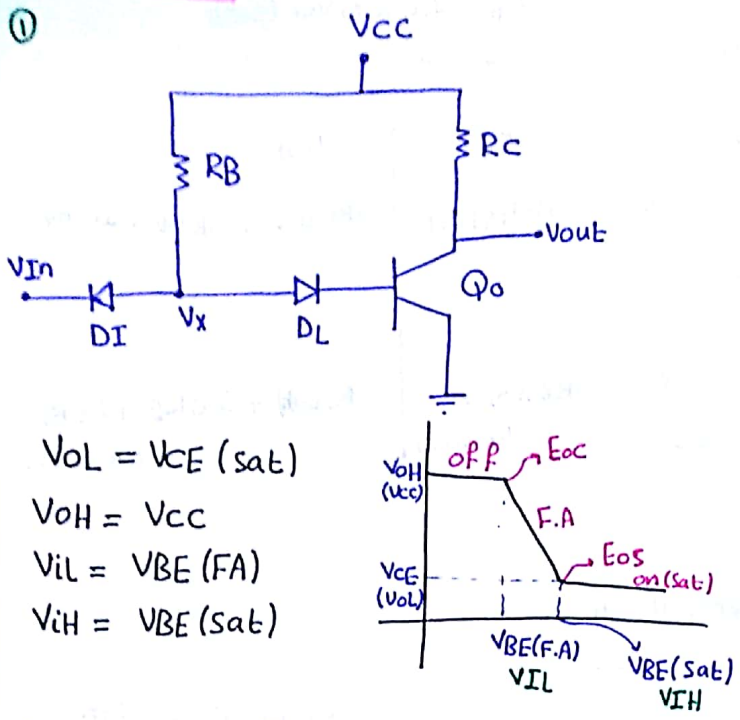
$\frac{V_{CC} - V_{CE(sat)} - V_{out}}{R_{CP}} = 2N \cdot \frac{V_{OH} - V_{BE(sat)}}{R_B}$

$R_{BO} = R_{BS}$

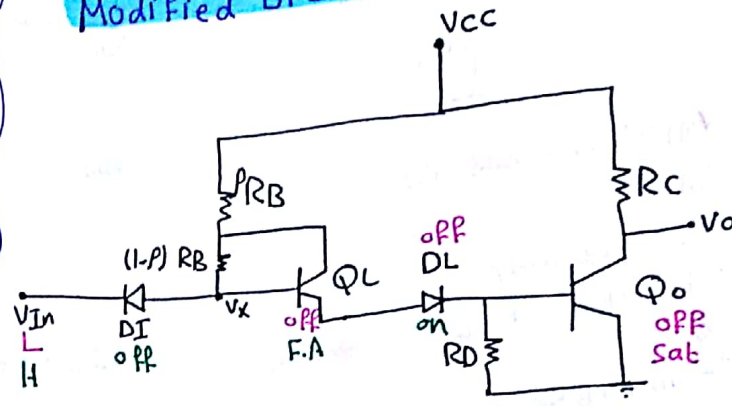
$N = \frac{V_{CC} - V_{CE(sat)} - V_{out}}{V_{out} - V_{BE(sat)}} \cdot \frac{R_B}{2 R_{CP}}$

(5)  $V_{out} = V_{iH}$

**Ch 6 :- DTL**

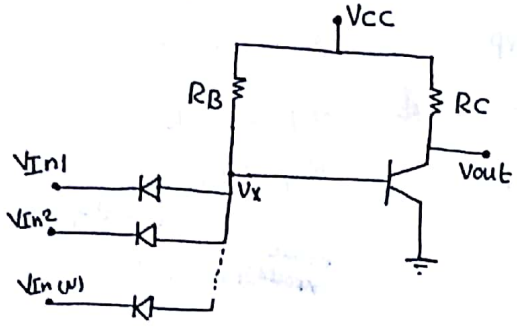


**④ Modified DTL :-**



$V_{oH} = V_{CC}$   
 $V_{oL} = 0$   
 $V_{iL} = 2V_{BE(FA)}$   
 $V_{iH} = V_{BE(FA)} + V_{BE(sat)}$

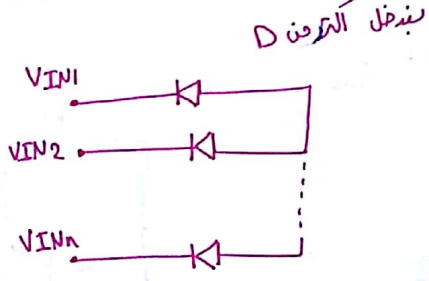
**② DTL NAND Gate:**



A	B	O/P
0	0	H
0	1	H
1	0	H
1	1	L

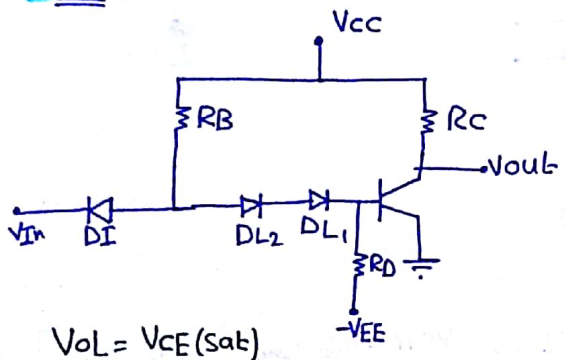
I/P si Low  
 2 diode activate  
 1 diode activate  
 diode 1

**⑤ NAND Gate**



V <sub>IN1</sub>	V <sub>IN2</sub>	O/P
L	L	H
L	H	H
H	L	H
H	H	L

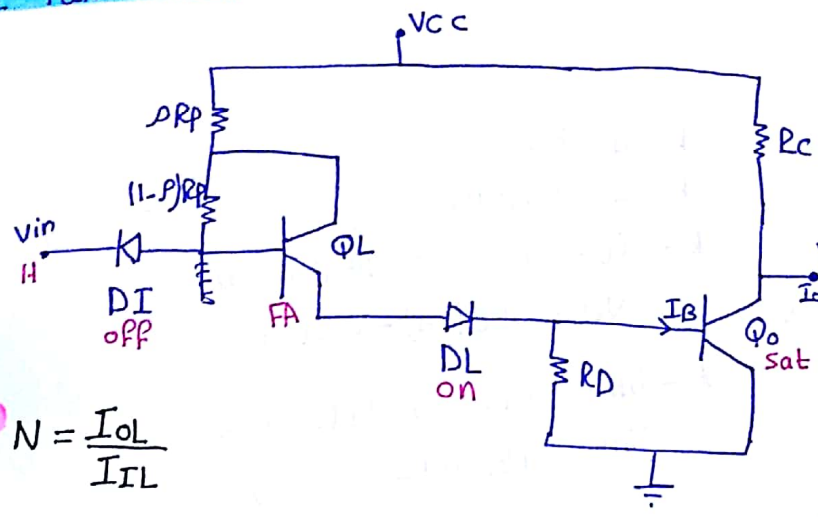
**③ 6.2**



$V_{oL} = V_{CE(sat)}$   
 $V_{oH} = V_{CC}$   
 $V_{iL} = V_{BE(FA)} + V_{D(on)}$   
 $V_{iH} = V_{BE(sat)} + V_{D(on)}$

(6)

**DTL Fan-out :-**



High عند O/P  
I/P

\*  $N = \frac{I_{OL}}{I_{IL}}$

\*  $-V_{CC} + R_B I_{IH} + V_{\gamma} + V_{CE(sat)} = 0$   
 $I_{IH} = \frac{V_{CC} - V_{\gamma} - V_{CE(sat)}}{R_B}$

\*  $I_{OL} = I_{CQ} - I_{RC}$   
 $I_{CQ} = \beta I_{BQ}$   
 $I_{BQ} = I_{E,Q} - I_{RD}$   
 $I_{E,Q} = I_{E,L} + I_{B,L}$   
 $I_{RD} = \frac{V_{BE(sat)}}{R_D}$   
 $I_{RC} = \frac{V_{CC} - V_{CE(sat)}}{R_C}$

\*  $-V_{CC} + \rho R_B I_E + I_{B,L} (1-\rho) R_B + V_{BE,L(FA)} + V_{DL(on)} + V_{BE,o(sat)} = 0$

\*  $I_{EL} = \frac{V_{CC} - V_{BE,L(FA)} - V_{DL(on)} - V_{BE(sat)}}{\rho R_B + \frac{(1-\rho) R_B}{\beta+1}}$   
 صيغة كثير اشتغال

**DTL power Dissipation**

$P_{CC(avg)} = \frac{I_{CC(OH)} + I_{CC(OL)}}{2} \cdot V_{CC}$

$I_{CC(OH)} = I_{R_{CQ}} + I_{\rho R_B} = I_{\rho R_B}$

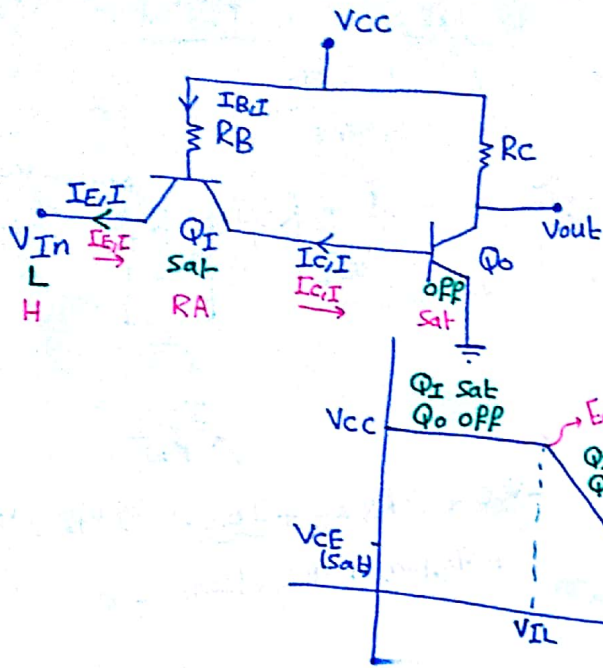
$I_{\rho R_B} = \frac{V_{CC} - V_{\gamma} - V_{in(Low)}}{R_B}$

$I_{CC(OL)} = I_{R_C} + I_{\rho R_B}$   
 $I_{R_C} = \frac{V_{CC} - V_{CE(sat)}}{R_C}$   
 $I_{\rho R_B} = \frac{V_{CC} - V_{BE(FA)} - V_{BE(sat)} - V_{\gamma}}{\rho R_B}$

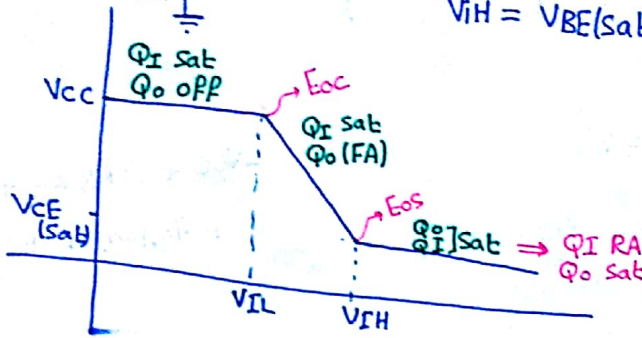
كانت تكبيراً كالمادة  
انه مع  $(1-\rho)R_B$   
يسهل صيغة كثير مقارنة  
فيها وبتجاهلها



# Ch7: TTL



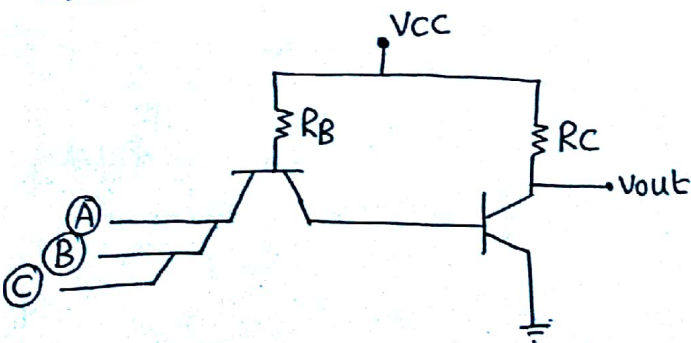
\*  $V_{OH} = V_{CC}$   
 \*  $V_{OL} = V_{CE(sat)}$   
 \*  $-V_{iL} - V_{CE(sat)} + V_{BE(FA)} = 0$   
 $V_{iL} = V_{BE(FA)} - V_{CE(sat)}$   
 \*  $-V_{iH} - V_{CE(sat)} + V_{BE(sat)} = 0$   
 $V_{iH} = V_{BE(sat)} - V_{CE(sat)}$



## \* Comparison between TTL and DTL

- ①  $D_I, D_L$  in DTL is replaced by  $Q_I$
- ② TTL has a higher Fan-out
- ③ TTL Faster than DTL
- ④  $I_{TTL} \gg I_{DTL}$
- ⑤ Less propagation delay time

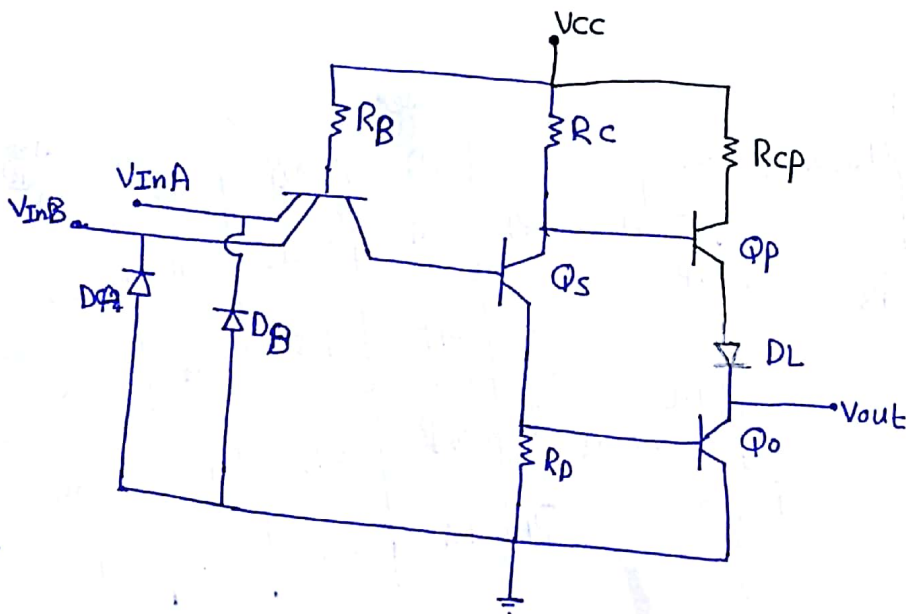
## TTL NOR:



A	B	O/P
L	L	H
L	H	L
H	L	L
H	H	L

=  $\overline{A+B}$

## Standard TTL:



- DA, DB For protection
- Q<sub>2</sub>: Logic inversion driving cct for Q<sub>3</sub>
- Q<sub>3</sub>, R<sub>cp</sub> pull up
- Q<sub>1</sub> pull down

$$R_c \gg R_{cp}$$

$$R_{cp} = 0.1 R_c$$

## Comparison between TTL (basic and Standard).

$$I_{\text{standard}} > I_{\text{basic}}$$

$$R_{cp} < R_c$$

Standard    basic

$$\tau_{\text{standard}} \ll \tau_{\text{basic}}$$

$$(R_{cp})(c)$$

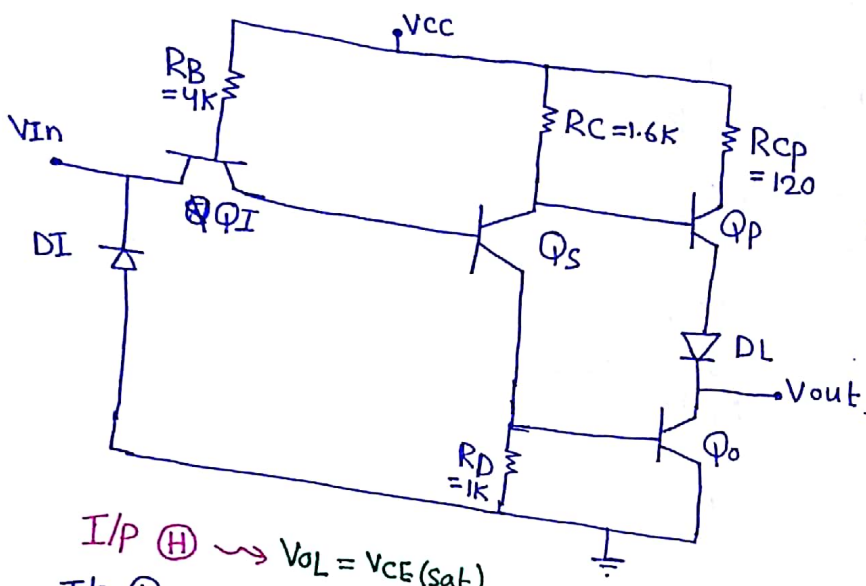
$$\frac{V_{CC} - V_{CE1P(\text{sat})} - V_{\gamma} - V_{CE1O(\text{sat})}}{R_{cp}}$$

$$(R_c)(c)$$

$$\frac{V_{CC} - V_{CE(\text{sat})}}{R_c}$$

Standard TTL NAND 01

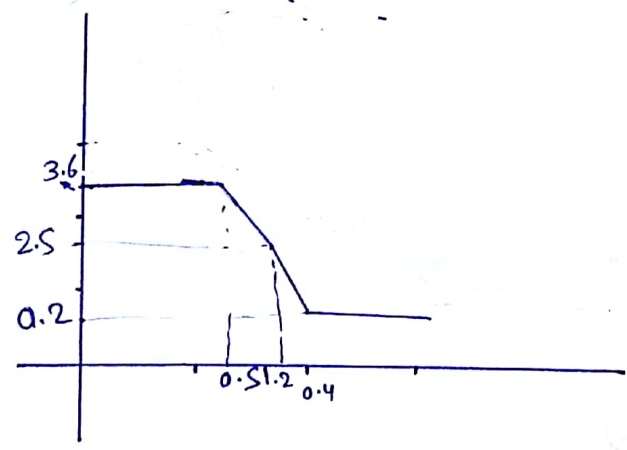
TTL Fan



	①	②	③	④
Q1	Sat	Sat	Sat	RA
Q2	OFF	FA	FA	Sat
Q3	OFF	OFF	FA	Sat
Q4	FA	FA	FA	OFF

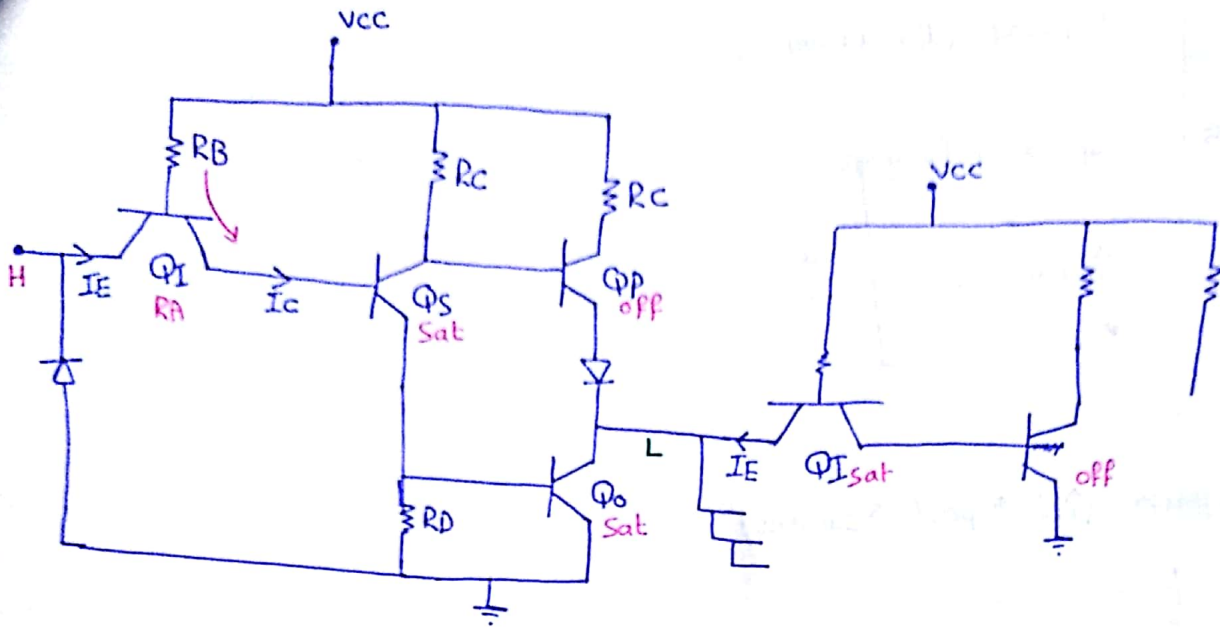
$I/P \text{ (H)} \rightarrow V_{OL} = V_{CE(sat)}$   
 $I/P \text{ (L)} \rightarrow V_{OH} = V_{CC} - V_{BE(FA)} - V_{\gamma}$   
 $= 5 - 0.7 - 0.7$   
 $= 3.6$

$* V_{OB} = V_{CC} - I_C R_C - V_{BE(P)} - V_{\gamma}$   
 $= 2.5$   
 $* V_{iL} = V_{BE(FA)} - V_{CE(sat)}$   
 $= 0.7 - 0.2$   
 $= 0.5$   
 $* V_{iH} = 2V_{BE(sat)} - V_{CE(sat)}$   
 $= 1.6 - 0.2$   
 $= 1.4$   
 $* V_{iB} = 2V_{BE(FA)} - V_{CE(sat)}$   
 $= 1.4 - 0.2$   
 $= 1.2$



*Handwritten scribble*

TTL Fan-out



بیشتر است  
High I/P

$$N = \frac{I_{OL}}{I_{IL}}$$

$$* I_{IL} = \frac{V_{CC} - V_{BE10(sat)} - V_{CE1(sat)}}{R_B}$$

$$* I_{OL} = \beta I_{B10}$$

$$* I_{B10} = I_{E1S} - \frac{V_{BE(sat)}}{R_D}$$

$$I_{B1S} + I_{C1S} = \frac{V_{CC} - V_{CE1S(sat)} - V_{BE10(sat)}}{R_C}$$

$$= I_{C1} = (1 + \beta) I_{B1}$$

$$= \frac{V_{CC} - V_{BE1} - 2V_{BE(sat)}}{R_B}$$

$V_{BC(RA)} = 0.7$

Power Dissipation:

$$P_{CC} = \frac{I_{CC(OH)} + I_{CC(OL)}}{2} * V_{CC}$$

$$* I_{CC(OH)} = I_{RB(OH)} + I_{RC(OH)} + I_{RE(OH)}$$

$$= \frac{V_{CC} - V_{BE1(sat)} - V_{In(low)}}{R_B}$$

$$* I_{CC(OL)} = I_{RB(OL)} + I_{RC(OL)} + I_{RE(OL)}$$

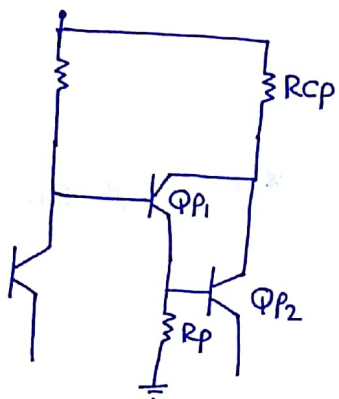
$$= \frac{V_{CC} - V_{BC1(RA)} - 2V_{BE(sat)}}{R_B} + \frac{V_{CC} - V_{CE10(sat)} - V_{BE10(sat)}}{R_C}$$

(11)

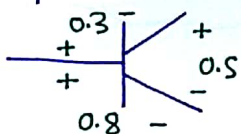
3 H FA  
(B-E) SBD

	Low power TTL LTTL	High speed TTL HS TTL
adv	↓ power	↑ power (dis advantage)
dis adv	↓ speed, ↓ P <sub>an out</sub>	↑ speed, ↑ current
	↓ current	↑ P <sub>an out</sub>
	↑ τ	↓ τ

\* Darlington pair: (↑N, ↑speed, ↑current)



Chapter 8 : STTL



$V_{SBD} = 0.3V$

to prevent reaching to sat mode we use Schottky diode (SBD)

\* operation mode :

1] off

(B-E) RA      (B-c) RA

SBD off  
Q off ] Q<sub>SBD</sub> off

$I_C = I_B = I_E = 0$

2] FA

(B-E) FA      (B-c) RA

SBD off  
Q FA ] Q<sub>SBD</sub> FA

$I_C = \beta I_B$

$I_E = (\beta + 1) I_B$

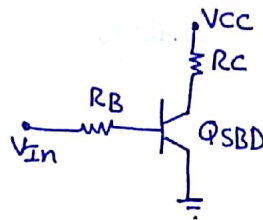
⇒ ③ HARD  
 (B-E) FA (B-c) FA  
 SBD on,  $Q_{on}$

$V_{BC} = V_{SBD} = 0.3$

$V_{BE}(\text{hard}) = 0.8$

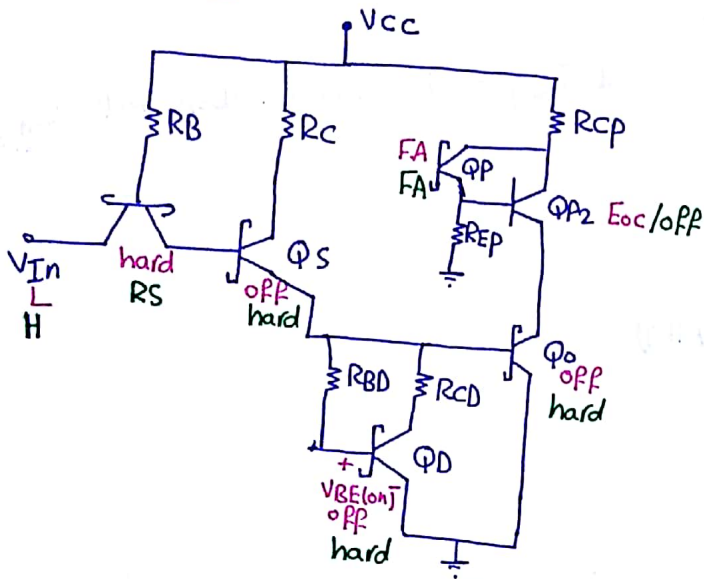
$V_{CE}(\text{hard}) = 0.5$

④ Reverse Schottky (RS)  
 (B-E) RA (B-c) FA  
 SBD on OFF ]  $Q_{SBD}(\text{RS})$



I/P (L) →  $Q_{SBD}$  OFF  $V_{oh} = V_{cc}$   
 I/P (H) →  $Q_{SBD}$  hard  
 $V_{ol} = V_{CE}(\text{hard}) = 0.5$   
 $V_{il} = V_{BE}(\text{FA}) = 0.7$   
 $V_{ih} = I_B R_B + V_{BE}(\text{hard})$   
 $\frac{I_C}{\beta} \rightarrow \frac{V_{cc} - V_{CE}(\text{sat})}{R_c}$

STTL



\*  $Q_D$ : pull down, Sink for the Load discharge path for  $Q_o$

\*  $Q_o$  and  $Q_D$  work at the same time

- \*  $V_{oh} = V_{cc} - 2V_{BE}(\text{FA})$
- \*  $V_{ol} = V_{CE}(\text{hard}) = 0.5$
- \*  $V_{il} = 2V_{BE}(\text{FA}) - V_{CE}(\text{sat})$
- \*  $V_{ih} = 2V_{BE}(\text{hard}) - V_{CE}(\text{hard})$

Fan-out :

High I/P

$N = \frac{I_{oL}}{I_{iL}}$

$I_{iL} = \frac{V_{cc} - V_{BE,i}(\text{hard}) - V_{CE,i0}(\text{hard})}{R_B}$

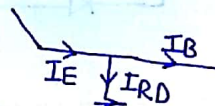
$I_{oH} = \beta I_{B,o}$

$I_{B,o} = I_{E,s} - I_{C,D}$

$\frac{V_{BE}(\text{hard}) - V_{CE,D}(\text{hard})}{R_{cD}} = I_R + V_{CE}(\text{hard}) - V_{BE}(\text{hard}) = 0$

$I_{B,s} + I_{C,s} \rightarrow \frac{V_{cc} - V_{CE,i,s}(\text{hard}) - V_{BE,i0}(\text{hard})}{R_c}$   
 $\frac{V_{cc} - V_{BC}(\text{RS}) - 2V_{BE}(\text{hard})}{R_B}$

neglect  $R_{BD}$  ( $E_{oo}$  small)



**Power dissipation:**

$I_{cc(OH)} = I_{RB} + I_{RC} + I_{RCP}$  → Neglect base current  
 I/P (L)

\*  $I_{RB} = \frac{V_{CC} - V_{BE,I(hard)} - V_{In(Low)}}{R_B}$

\*  $I_{RCP} = \frac{V_{CC} - V_{BE,P(FA)}}{R_{EP}}$

$I_{cc(OL)} = I_{RB} + I_{RC} + I_{RCP}$

\*  $I_{RB} = \frac{V_{CC} - V_{Bc(Rs)} - 2V_{BE(hard)}}{R_B}$

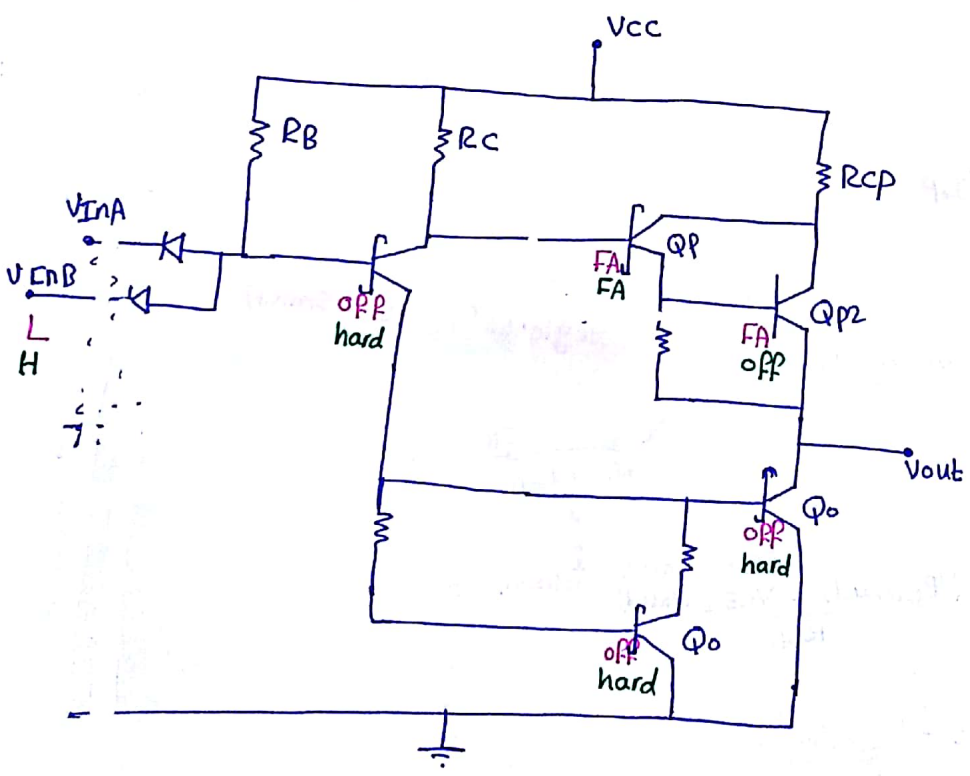
\*  $I_{RC} = \frac{V_{CC} - V_{CE,s(hard)} - V_{BE,o(hard)}}{R_C}$

\*  $I_{RCP} = \frac{V_{CE,s(hard)} + V_{BE,o(hard)} - V_{BE,P(FA)}}{R_{EP}}$

- 0 - IR - VBE (FA) + VCE (hard) + VBE,o (hard) = 0

$I_{REP} = \frac{V_{CE,s(hard)} + V_{BE,o(hard)} - V_{BE,P(FA)}}{R_{EP}}$

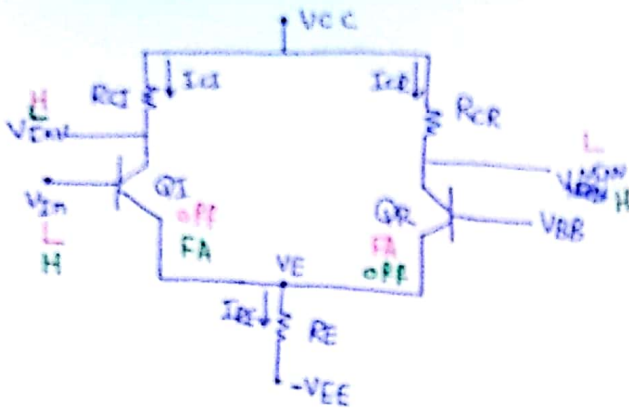
**18STTL:**



Replace VBE  
 Q3 w  
 →  
 2 Schottky diode

## Second:

### Chapter 11: (ECL)



$$* I_{RE} = \frac{V_E + V_{EE}}{R_E}$$

$$* V_E = V_{in} - V_{BE, I} \text{ (if } Q_I \text{ on)}$$

$$* V_E = V_{BB} - V_{BE, R} \text{ (if } Q_R \text{ on)}$$

$$* V_{inV} = V_{CC} - I_{C1} R_{C1}$$

$$* V_{inV} = V_{CC} - I_{C2} R_{C2}$$

$$V_{BE} (FA) = V_{BE} (ECL) = 0.75$$

#### \* I/P (Low)

$$V_{in} < V_{BB} \quad Q_I \text{ (off)} \\ Q_R \text{ (FA)}$$

$$I_E = \frac{V_{BB} - V_{BE} (ECL) + V_{EE}}{R_E}$$

$$I_{C1} = 0$$

No voltage drop in  $R_{C1}$ .

#### \* I/P (High)

$$V_{in} > V_{BB} \quad Q_I \text{ (FA)} \\ Q_R \text{ (off)}$$

$$I_E = \frac{V_{in} - V_{BE} (ECL) + V_{EE}}{R_E}$$

$$I_{C2} = 0$$

$$* V_{in} < V_{BB} \text{ is not valid} \\ Q_I \rightarrow \text{off}$$

$$V_{BE, I} = V_{in} - V_E \\ (V_{BB} + V_{BE, R}) \\ = \frac{V_{in} - V_{BB} + V_{BE, R}}{-V_C}$$

$$V_{BE} < V_{BE} (ECL)$$

$\Rightarrow Q_I$  off

$$V_{IH} = V_{BB} + 0.05$$

$$V_{IL} = V_{BB} - 0.05$$

$$* V_{in} = V_{BB} \text{ is not valid} \\ Q_I, Q_R \text{ both on}$$

$$I_{C2} = I_{RE} = \frac{V_{BB} - V_{BE, R} (ECL) + V_{EE}}{R_E}$$

$$I_{C1} = I_{RE} = \frac{V_{in} - V_{BE, I} (ECL) + V_{EE}}{R_E}$$

$$I_{RE} = I_{E, I} + I_{E, R}$$

$$I_{E, I} = I_{E, R}$$

$$I_{E, I} = I_{E, R} = \frac{I_{RE}}{2}$$

$$* V_{in} > V_{BB} \text{ is not valid} \\ Q_I \text{ on}$$

$$V_{BE, R} = V_{BB} - V_E \\ (V_{in} - V_{BE, I} (ECL))$$

$$\text{if } V_{in} > V_{BB} + 0.05$$

$$V_{BE, R} = V_{BB} - V_{BB} - 0.05 + V_{BE, I}$$

$$V_{BE, R} < V_{BE, I} (ECL) - 0.05$$

$\therefore Q_R$  off



⇒  $V_{inv}$  at  $V_S$

When I/P ↑,  $Q_I$  becomes sat

$Q_R$  Remains off

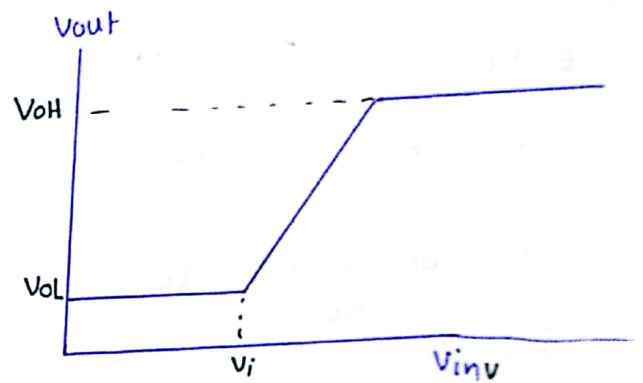
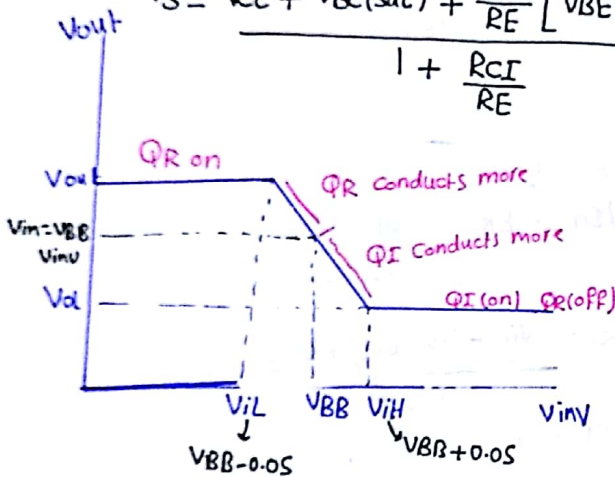
$$1) V_{inv} = V_{CC} - \frac{I_{C1} R_{C1}}{RE} = \frac{V_S - V_{BE, I(sat)} + V_{EE}}{RE}$$

$$2) V_{inv} = V_S - V_{BC(sat)}$$

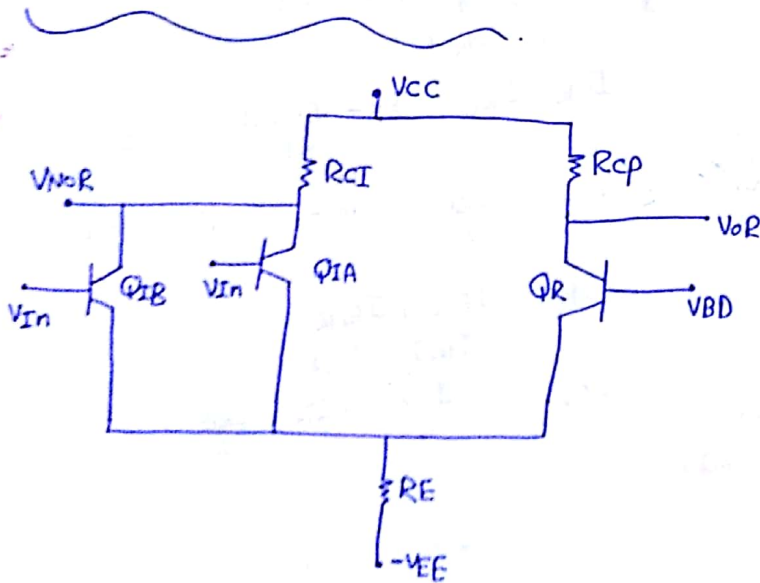
when solving 1 in 2

$$V_S = V_{CC} + V_{BC(sat)} + \frac{R_{C1}}{RE} [V_{BE(sat)} - V_{EE}]$$

$$1 + \frac{R_{C1}}{RE}$$

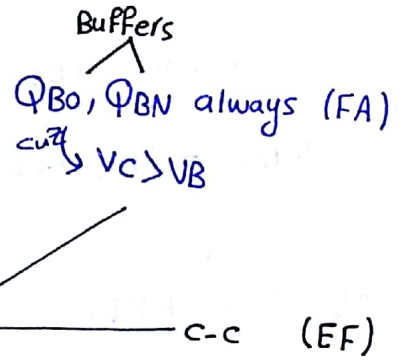
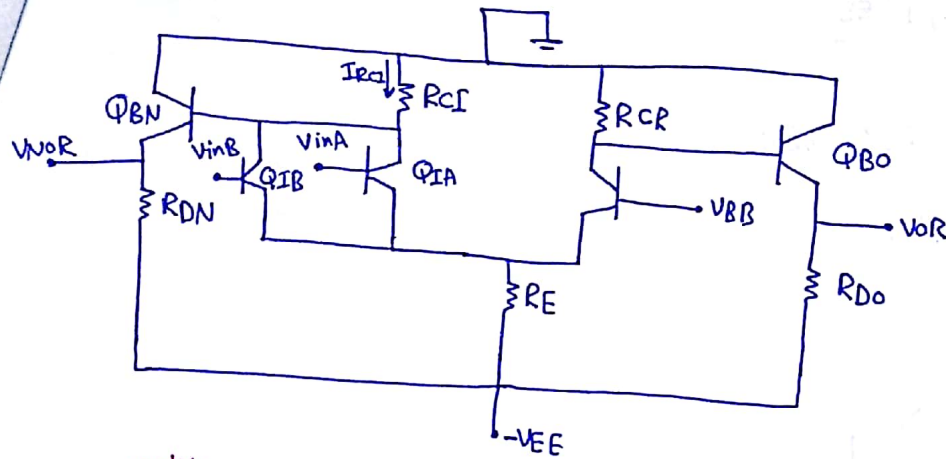


(Transition width = 0.1)  
 $V_{IH} - V_{IL} = 0.1$



A	B	oR	NoR
0	0	1	0
0	1	0	1
1	0	0	1
1	1	0	1

11.5: MECL OR/NoR gate



adv:  
 ↑ current at o/p  
 ↑ N (Fan-out)  
 ↑ speed  
 I/p, o/p swing Compatible

dis adv:  
 ↑ power  
 ↑ Switching Spikes due to high Speed.

- \* \$R\_{DN}, R\_{DO}\$ : ① passive pull down ckt  
 ② loads for the buffers
- \$I\_{vin} < I\_{B\beta}\$
- 1) \$R\_{CI} < R\_{CR}\$  
 \$I\_{vin} < I\_{VBB}\$
- 2) \$R\_{CI} > R\_{CR}\$

MECL (NoR)

① \$V\_{in} < V\_{BB}\$, \$Q\_I\$ off, \$Q\_R\$ on

الكل يكون هيلك بغالة هيكه لا يتجاوب  
 ابا اذا هيكه يتجاوب بتصير \$I\_C = I\_B = 0\$

$$0 + I_{RCI} (R_{CI}) + V_{BE,RN} (E_{CL}) + V_{NoR} = 0$$

$$V_{OH} = -I_{RCI} (R_{CI}) - V_{BE,RN} (E_{CL})$$

$$I_{RCI} = I_{B,BN}$$

$$-0 + R_{CI} \underbrace{I_{RCI}}_{I_{B,BN}} + V_{BE,RN} (E_{CL}) + (1+\beta) I_{B,BN} R_{DN} - V_{EE} = 0$$

$$I_{B,BN} = \frac{V_{EE} - V_{BE,RN} (E_{CL})}{R_{CI} + R_{DN} (1+\beta)}$$

$$V_{iL} = V_{BB} - 0.05$$

$$V_{iH} = V_{BB} + 0.05$$

②  $V_{in} > V_{BB}$  ,  $Q_I$  FA ,  $Q_R$  OFF

$$I_{RC,I} = I_{RE} = \frac{V_{in} - V_{BE}(ECL) + V_{EE}}{R_E}$$

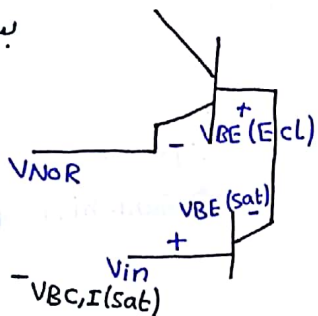
Ignore  $I_{B,BN}$  when  $I_{CI} > I_{B,BN}$

$$V_{NOR} = -I_{RCI} R_{CI} - V_{BE,BN}(ECL)$$

at  $V_S$  ,  $V_{NOR}(V_S)$

$$V_{BE}(sat) \leftarrow V_{BE}(ECL) \text{ due}$$

$$-V_{NOR} - V_{BE}(ECL) + V_{BC}(sat) + V_{in} = 0$$



$$\textcircled{3} \frac{V_{NOR}}{R_{CI}} = \frac{V_{in} - V_{BE,BN}(ECL) - V_{BC,I}(sat)}{R_E}$$

$$\textcircled{1} I_{RC} = I_{RE} = \frac{V_S - V_{BE}(sat) + V_{EE}}{R_E}$$

$$\textcircled{2} V_{NOR} = V_{out} = -I_{RCI} R_{CI} - V_{BE,BN}(ECL)$$

Solve ② and ③ for  $V_S$

$$V_S = \frac{V_{BC}(sat) + \frac{R_{CI}}{R_E} [V_{BE}(sat) - V_{EE}]}{1 + \frac{R_{CI}}{R_E}}$$

$$* V_{NMH} = V_{OH} - V_{IH}$$

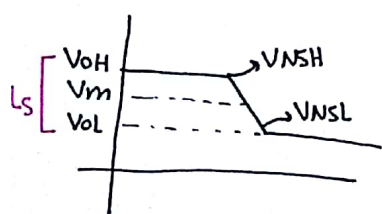
$$* V_{NML} = V_{IL} - V_{OL}$$

$$\text{Transition width} = V_{IH} - V_{IL}$$

### Noise Sensitivity

$$V_{HNS} = V_{OH} - V_m$$

$$V_{LNS} = V_m - V_{OL}$$



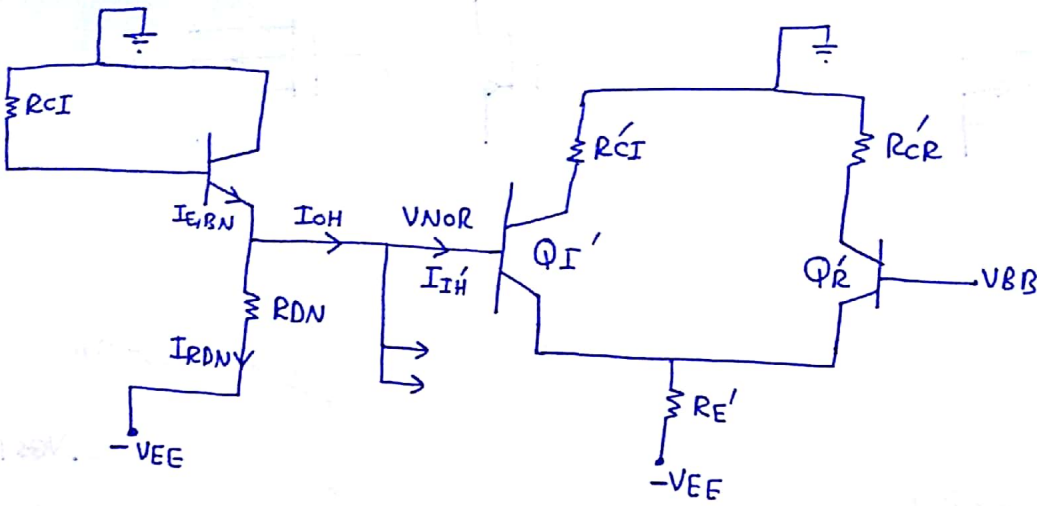
$$L_S = V_{OH} - V_{OL}$$

### Noise immunity

$$V_{NIH} = \frac{V_{NSH}}{L_S}$$

$$V_{NIL} = \frac{V_{NSL}}{L_S}$$

Fan-out MECL(2)



$$N = \frac{I_{oH}}{I_{iH}}$$

L(I/P) → H(O/P)

$$* I_{iH}' = \frac{I_{RE}}{\beta + 1} = I_{B,I} = \frac{I_E}{\beta + 1}$$

$$* I_{RE} = \frac{V_{oH} - V_{BE,I}(ECL) + V_{EE}'}{R_{E}'}$$

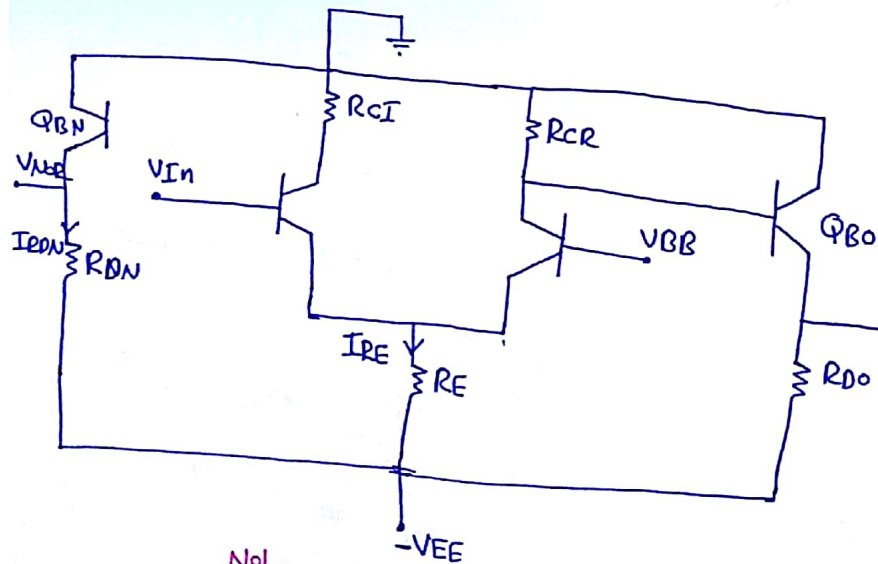
$$* I_{oH} = I_{E,BN} - I_{RDN}$$

$$\rightarrow I_{E,BN} = (1 + \beta) I_{B,BN}$$

$$\rightarrow I_{B,BN} = \frac{0 - V_{BE,BN}(ECL) - V_{oH}}{R_{CI}} (\beta + 1)$$

$$I_{RDN} = \frac{V_{oH} + V_{EE}}{R_{DN}}$$

ECL power Dissipation



$$* I_{EE(NoH)} = I_{RE(NoH)} + I_{RDN(NoH)} + I_{RDo(NoH)}$$

$$* I_{RE} = \frac{V_{BB} - V_{BE,I}(ECL) + V_{EE}}{R_E}$$

$$* I_{RDN} = \frac{V_{oH} + V_{EE}}{R_{DN}}$$

$$V_{oH} = -I_{RCI} R_{CI} - V_{BE,BN}(ECL)$$

$$* I_{RDo} = \frac{V_{oL} + V_{EE}}{R_{Do}}$$

$$V_{oL} = -I_{RCR} R_{CR} - V_{BE}(ECL)$$

$$* I_{EE(OL)} = I_{RE(OL)} + I_{RDN(OL)} + I_{RDo(OL)}$$

$$= \frac{V_{in} - V_{BE,I}(ECL) + V_{EE}}{R_E} + \frac{V_{oL} + V_{EE}}{R_{DN}} + \frac{V_{oH} + V_{EE}}{R_{Do}}$$

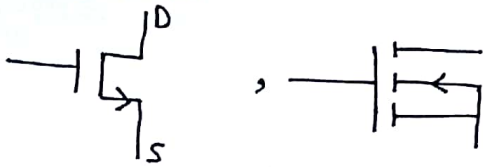
$$P_{avg(EE)} = V_{EE} \left[ \frac{I_{EE(oH)} + I_{EE(oL)}}{2} \right]$$

(19)

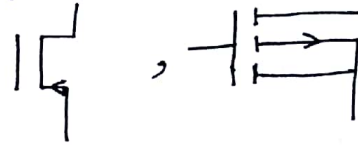
لو امكن في Vcc في الـ Super-position  
في الـ EE في الـ Vcc

# Chapter 16:

## NMOS



## PMOS



### \* NMOS operations:

①  $V_{GS} < V_{TN}$   
NMOS off,  $I_D = 0$

②  $V_{GS} > V_{TN}$

a)  $V_{DS} < V_{DS(sat)}$

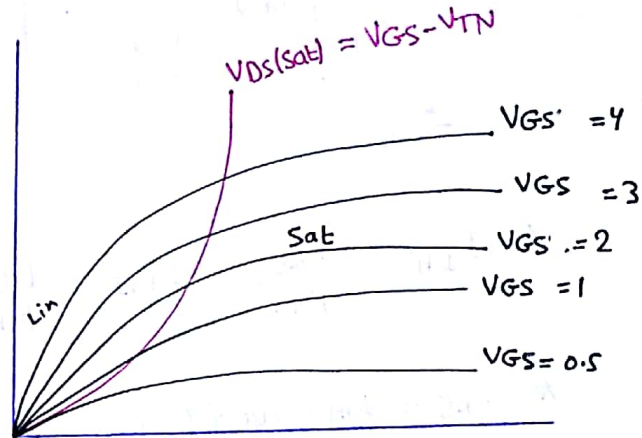
NMOS Linear

$$I_D(\text{lin}) = k_n \left[ (V_{GS} - V_{TN})V_{DS} - \frac{V_{DS}^2}{2} \right]$$

b)  $V_{DS} > V_{DS(sat)}$

NMOS Sat

$$I_D(\text{sat}) = \frac{k_n}{2} [V_{GS} - V_{TN}]^2$$



$$* k_n = \frac{\mu_n C_{ox}}{L} \frac{W}{L} = k_n' \frac{W}{L}$$

$$* C_{ox}' = \frac{\epsilon_{ox}}{\epsilon_{ox}}$$

## PMOS:

①  $V_{SG} < -V_{TP}$   
PMOS off

②  $V_{SG} > -V_{TP}$

a)  $V_{SD} < V_{SD(sat)}$

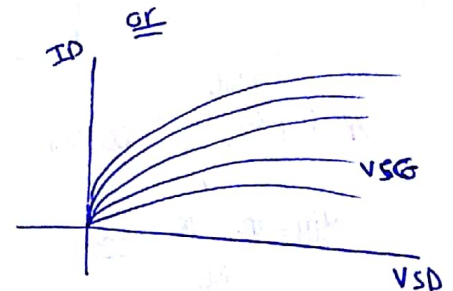
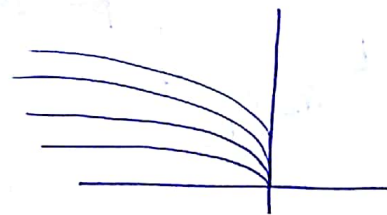
$$V_{SD(sat)} = V_{SG} + V_{TP}$$

$$I_{DP} = k_p \left[ (V_{SG} + V_{TP})V_{SD} - \frac{V_{SD}^2}{2} \right]$$

b)  $V_{SD} > V_{SD(sat)}$

$$I_{DP} = \frac{k_p}{2} [V_{SG} + V_{TP}]^2$$

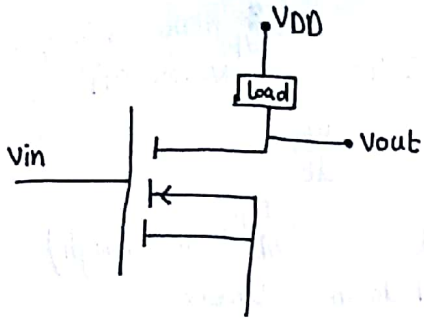
PMOS Sat



$$* k_p = \frac{\mu_p C_{ox}}{L} \frac{W}{L} = k_p' \frac{W}{L}$$

$$\frac{V_{SD} I_{DP}}{MA} \frac{1}{V^2}$$

Chapter 17 :-



\*  $V_{GS} > V_{TN}$   
NMOS Linear

$V_{GS} < V_{TN}$   
NMOS off

\*  $R_d$  is  $I_d$  ...  
To Let  $I_D = 0 \rightarrow R_L \rightarrow \infty$   
 $V_{DS} \approx 0$

$I_D = 0$  when  $V_{DS} = 0$  only

\* NMOS is used as pull down in active mode

\*  $R_{DS}$  is  $R$  (Load)  
(channel)

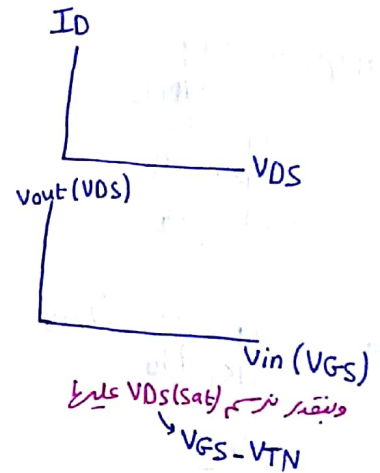
channel Resistance  
\*  $R_{DS} = \frac{dV_{DS}}{dI_D}$

if  $I_D = I_{D(Lin)}$   
 $\frac{1}{R_{DS}} = \frac{dI_D}{dV_{DS}} = k_n [V_{GS} - V_{TN} - V_{DS}]$

$$R_{DS} = \frac{1}{k_n [V_{GS} - V_{TN} - V_{DS}]}$$

$V_{DS} \downarrow, R_{DS} \downarrow, \text{Conductivity} \uparrow$

$$V_{DS} = V_{DD} - I_D R_L \begin{cases} \rightarrow I_D = 0 \\ \rightarrow V_{DS} = 0 \end{cases}$$



$$P_{stat} = \frac{I_{DD(OH)} + I_{DD(OL)}}{2} \cdot V_{DD}$$

$$P_{dyn} = C_L \cdot \frac{V_{DD}}{Freq}$$

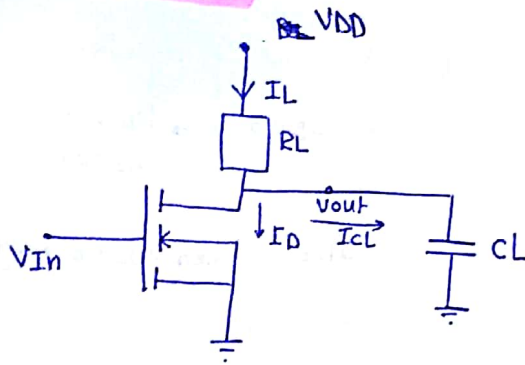
$$P_{total} = P_{stat} + P_{dyn}$$

$Freq \uparrow, \text{time} \downarrow, \text{Switching Fast}$

$$I_{dis} \ll I_{charge}$$

$R_{DS} \downarrow, V_{DS} \downarrow, \text{Conductivity} \uparrow$

## Fan-out :



\* when I/p (Low)

$$V_{GS} < V_{TN}$$

(I/p high  $\rightarrow$  Low)  
NMOS off

$$I_L = I_{CL} = C_L \frac{dV_C}{dt}$$

\* when I/p (high)

(I/p Low  $\rightarrow$  high)

NMOS pull down, Linear

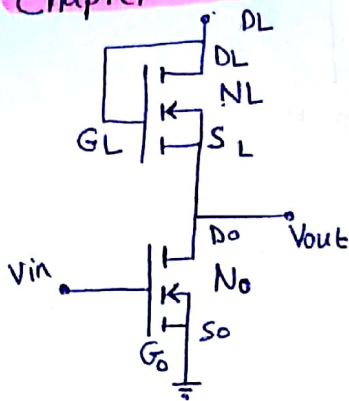
$$I_{dis} = -I_{CL} = -C_L \frac{dV_C}{dt} = -(I_L - I_D)$$

$$I_{CL} = I_L - I_D$$

$$I_{CL} = C_L \frac{dV}{dt}$$

$$I_{dis} = -C_L \frac{dV}{dt}$$

## Chapter 19 :



NL  $\Rightarrow$  Load  
No  $\Rightarrow$  MOSFET

\*  $V_{DS,L} = V_{GS,L}$  because  $G_o, G_L$  are connected

$$* V_{DSL(sat)} = V_{GS,L} - V_{TL}$$

$V_{DSL} > V_{DSL(sat)}$  NMOS sat

$$I_{DL} = I_{Do}$$

$$* V_{out} = V_{Dso} = V_{DD} - V_{DS,L}$$

$$V_{DS,L} = V_{DD} - V_{Dso} = V_{GS,L}$$

\* VoH if  $V_{in} = V_{GS,o} < V_{TN}$   
No is off

$$I_{D,o} = I_{D,L} = 0$$

$$V_{DS,o} = V_{DD} - V_{DS,L} \quad \leftarrow V_{GS,L}$$

$$V_{DS,L} = V_{GS,L} = V_{TL}$$

$$V_{DS,o} = V_{OH} = V_{DD} - V_T$$

NL  $\rightarrow$  sat

\* VoL

$V_{in} \geq V_{To}$  (high)

$V_{out}$  at vm  $V_{DS,o} \geq V_{DS,o(sat)}$

NL, No both sat

$$I_{DL(sat)} = I_{Do(sat)}$$

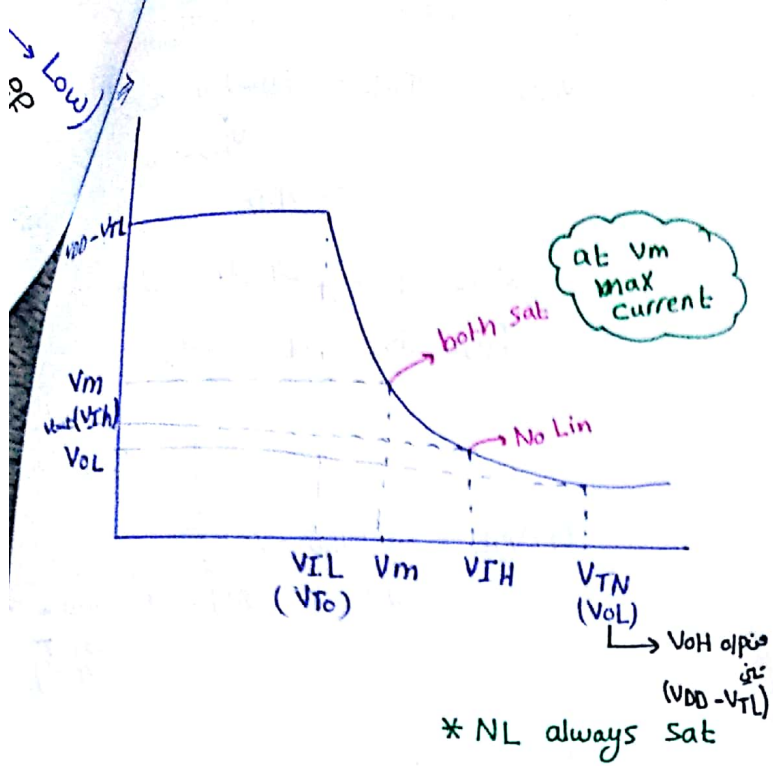
$$\textcircled{1} \frac{K_L}{2} [V_{GS,L} - V_{TL}]^2 = \frac{K_o}{2} [V_{GS,o} - V_{To}]^2$$

$$\textcircled{2} V_{GS,L} = V_{DS,L} = V_{DD} - V_{out}$$

$$\textcircled{3} V_{GS,o} = V_{IN}$$

$\textcircled{2}$  and  $\textcircled{3}$  in  $\textcircled{1}$

$$V_{out} = -\sqrt{\frac{K_o}{K_L}} V_{IN} + V_{To} \sqrt{\frac{K_o}{K_L} + V_{DD} - V_{TL}}$$

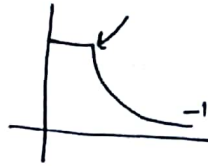


o/p drops with slope  $-\sqrt{\frac{K_o}{K_L}}$   
 The larger the  $-\sqrt{\frac{K_o}{K_L}}$ , the steeper the transition

\* at midpoint  $V_{In} = V_{out} = V_m$  (Both sat)

$$V_m + \sqrt{\frac{K_o}{K_L}} V_m = V_{DD} - V_{TL} + V_{T0} \sqrt{\frac{K_o}{K_L}}$$

$$V_m = \frac{V_{T0} \sqrt{\frac{K_o}{K_L}} + V_{DD} - V_{TL}}{1 + \sqrt{\frac{K_o}{K_L}}}$$



\* لا يوجد  $V_{OL}$  تقريبا  
 $N_L(\text{sat}) = N_o(\text{Lin})$   
 $I_{DL}(\text{sat}) = I_{D_o}(\text{Lin})$

$$\frac{K_L}{2} (V_{GS,L} - V_{TL})^2 = K_o \left[ (V_{GS,o} - V_{T0}) V_{DS,o} - \frac{V_{DS,o}^2}{2} \right]$$

$\downarrow$   $V_{DS,L} = V_{DD} - V_{out}$        $\downarrow$   $V_{IN} = V_{DD} - V_{TL}$        $\downarrow$   $V_{out}$

$$V_{OL} = \frac{K_L (V_{DD} - V_{TL})^2}{2 K_L (V_{DD} - V_{TL}) + 2 K_o (V_{DD} - V_{TL} - V_{T0})}$$

$V_{i,L} = V_{T0}$



\*  $V_{IH} \approx V_{OL}(V_{IH})$  لا يتساوى

Slope of  $V_{IH} = \frac{dV_{out}}{dV_{in}} = -1$

1)  $I_{DL}(sat) = \frac{K_L}{2} (V_{GS,L} - V_{TL})^2 = \frac{K_L}{2} (V_{DD} - V_{out} - V_{TL})^2$

2)  $dI_d(V_{out}) = \frac{dI_d}{dV_{out}} dV_{out}$

3)  $\frac{dI_d}{dV_{out}} = -K_L (V_{DD} - V_{out} - V_{TL})$

4)  $I_{D(Lin)} = K_D [(V_{GS} - V_{TN}) V_{DS} - \frac{V_{DS}^2}{2}]$   
 $V_{in}$   $V_{out}$

5)  $dI_{D0} = \frac{dI_{D0}}{dV_{in}} dV_{in} + \frac{dI_{D0}}{dV_{out}} dV_{out}$

6)  $K_D V_{out}$

7)  $K_D (V_{IN} - V_{T0} - V_{out})$

Linear = Sat نحوى مستقيم

$dI_{DL}(Sat) = dI_{D0}(Lin)$

$\frac{dI_{DL}}{dV_{out}} dV_{out} = \frac{dI_{D0}}{dV_{in}} dV_{in} + \frac{dI_{D0}}{dV_{out}} dV_{out}$

$dV_{out} (\frac{dI_{DL}}{dV_{out}} - \frac{dI_{D0}}{dV_{out}}) = \frac{dI_{D0}}{dV_{in}} dV_{in}$

$\frac{dV_{out}}{dV_{in}} = \frac{\frac{dI_{D0}}{dV_{in}}}{(\frac{dI_{DL}}{dV_{out}} - \frac{dI_{D0}}{dV_{out}})} = -1$  (8)

3, 6, 7 in 8 نحوى

$V_{out}(V_{IH}) = \frac{K_D (V_{IN} - V_{T0}) + K_L (V_{DD} - V_{TL})}{2K_D + K_L}$

\*  $V_{in}(V_{IH}) = V_{T0} + \frac{2(V_{DD} - V_{TL})}{\sqrt{\frac{3K_D}{K_L}} + 1}$

⇒ at  $I_D = 0$

$V_{DS,0} = V_{DD} - V_{DS,L}$

$V_{GS,L} = V_{DSL} = V_{TL}$

$I_{DL} = I_{D0} = 0$

$V_{DS,0} = V_{DD} - V_{TL} = V_{OH}$

\* at  $V_{DS} = 0$

$V_{GS,L} = V_{DSL} = V_{DD} - V_{out} = 0$   
 $V_{DS,0} = 0$   
 $= V_{DD}$

\* لا استخراج القيمة من الرسمة نخرج

$I_{D,0}(Lin) = I_{D,L}(Sat)$

المطلوب:

①  $V_{OL} = \frac{K_L (V_{DD} - V_{TL})^2}{2K_L (V_{DD} - V_{TL}) + 2K_D (V_{DD} - V_{TL})}$

②  $V_{OH} = V_{DD} - V_{TL}$

③  $V_{IL} = V_{GS,0}$

④  $V_{IH} = V_{T,0} + \frac{2(V_{DD} - V_{TL})}{\sqrt{\frac{3K_D}{K_L}} + 1}$

⑤  $V_m = \frac{V_{DD} - V_{TL} + \sqrt{\frac{K_D}{K_L}} V_{T,0}}{1 + \sqrt{\frac{K_D}{K_L}}}$

⑥  $V_{out}(V_{IH}) = \frac{K_L (V_{DD} - V_{TL}) + K_D (V_{IH} - V_{T,0})}{2K_D + K_L}$

power dissipation:

$P_{total} = P_{stat} + P_{dyn}$

$P_{dyn} = N C_L V_{DD}^2$

$P_{stat} = V_{DD} - \frac{I_{DD(OL)} + I_{DD(OH)}}{2}$

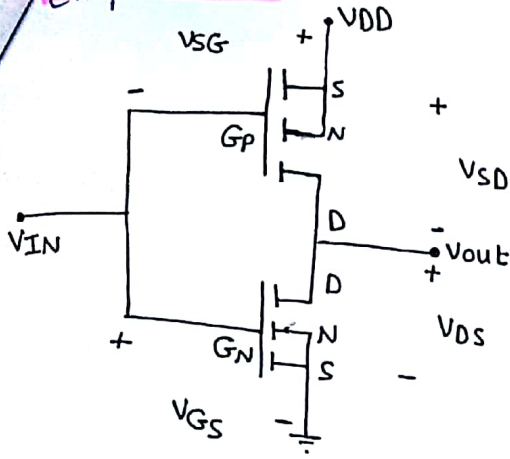
\*  $I_{DD(OH)}$  I/p (L)

$I_{DL}(sat) = I_{D0}(OFF) = 0$

\*  $I_{DD(OL)}$  I/p high

$I_{D0}(Lin) = I_{DL}(Sat)$

Chapter 23:



$V_{in}$	$G_p$	$G_n$
L	Lin	off
H	off	Lin

\* I/p (Low) ,  $V_{oH}$   $> V_{TP}$

$V_{in} = 0$  ,  $V_{GS} = 0 < V_{TN} \rightarrow N_o(off)$

$V_{SG} = V_{DD} - V_{IN} = V_{DD}$

$V_{SG}, V_{DD} > -V_{TP} \rightarrow P_o(Lin)$

$V_{SD}(sat) = V_{SG} + V_{TP}$

$V_{SD}(sat) = V_{DD} + V_{TP}$

$V_{SD} < -V_{SD}(sat)$   
(Lin)

$I_{DN}(off) = I_{DP}(Lin)$

$I_D = 0$  / when  $V_{SD} = 0$

$V_{SDS} = V_{DD} - V_{SD} = V_{DD} = V_{oH}$

$V_{oH} = V_{DD}$

$V_{oH} \rightarrow V_{iL} \rightarrow N_o off \rightarrow I_{DP}, I_{DN} = 0 \rightarrow V_{DS} = 0$

$V_{DS} = V_{DD} - V_{out}$

$V_{out} = V_{DD}$   
 $V_{oH} = V_{DD}$

\* I/p (high) ,  $V_{in} = V_{DD}$

$N_o, Lin$

$P_o, off$

$V_{GS} = V_{DD}$

$V_{SG} = V_{DD} - V_{in}$

$= V_{DD} - V_{in} = 0$

$V_{DD} > V_{IN}$

$0 < -V_{TP}$   
off

$I_{DN}(Lin) = I_{DP}(off)$

\*  $I_{DN}$  is 0 when  $V_{DS} = 0$

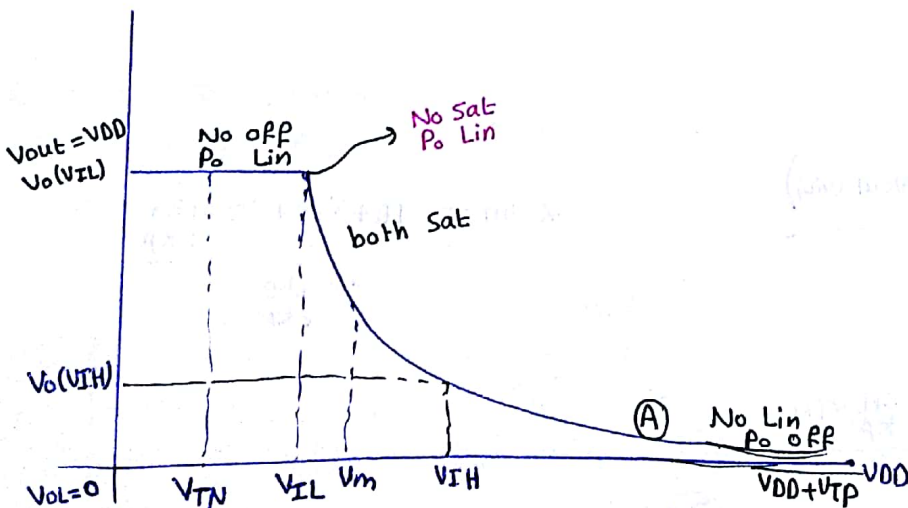
$V_{oL} = 0$

$V_{oL} \rightarrow V_{iH} \rightarrow P_o off$

$I_D = 0 \rightarrow V_{DS} = 0$

$V_{out} = V_{DS} = 0$

$V_{oL} = 0$



⇒ at (A)

when  $P_o$  turns off

$$V_{SG} = V_{DD} - V_{IN}$$

For  $P_o$  to be on

$$V_{SG} > -V_{TP}$$

$$V_{DD} - V_{IN} > -V_{TP}$$

$$-(-V_{IN}) > -V_{TP} - V_{DD}$$

$$V_{IN} < V_{TP} + V_{DD}$$

$$\left[ \begin{array}{l} V_{SG} < -V_{TP} \\ V_{IN} > V_{DD} + V_{TP} \end{array} \right]$$

off  $\omega$   $P_o$   $\bar{\omega}$

To find  $V_{IL}$

$P_o$  Lin, No Sat

$$I_{Dp_o}(Lin) = I_{Dn_o}(Sat)$$

$$K_p \left[ \frac{(V_{SG} + V_{TP})V_{SD} - \frac{V_{SD}^2}{2}}{V_{DD} - V_{in}} \right] = \frac{K_n}{2} * \left[ \frac{(V_{GS} - V_{TN})^2}{V_m} \right]$$

$$dI_{DN} = dI_{DP}$$

$$\frac{dI_{DN}}{dV_{in}} dV_{in} = \frac{dI_{DP}}{dV_{in}} dV_{in} + \frac{dI_{DP}}{dV_{out}} dV_{out}$$

$$V_{in} - V_{GS,0} = K_p V_{SD,p} + K_p (V_{SG,p} + V_{TP}) - K_p (V_{SG} + V_{TP}) - V_{out}$$

$$V_{IL} = \frac{2 V_{out}(V_{IL}) - V_{DD} + V_{TP} + \frac{K_n}{K_p} V_{TN}}{1 + \frac{K_n}{K_p}}$$

$$V_{OL} = 0$$

$$* V_{OH} = V_{DD}, V_{OL} = 0$$

$$* V_{IH} = \frac{V_{DD} + V_{TP} + \frac{K_n}{K_p} (V_{TN} + 2V_{out}(V_{IL}))}{1 + \frac{K_n}{K_p}}$$

$$* V_m = \frac{V_{DD} + V_{TP} + V_{IN} \sqrt{\frac{K_n}{K_p}}}{1 + \sqrt{\frac{K_n}{K_p}}}$$

$$* V_{IL} = \frac{2 V_{out}(V_{IL}) - V_{DD} + V_{TP} + \frac{K_n}{K_p} V_{TN}}{1 + \frac{K_n}{K_p}}$$

⇒ \* mid point  $V_{in} = V_{out} = V_m$

$$I_{DN}(Sat) = I_{DP}(Sat)$$

$$\frac{k_n}{2} (V_m - V_{TN})^2 = \frac{k_p}{2} \left[ \frac{V_{SG,P}}{V_{DD} - V_m} + V_{TP} \right]^2$$

$$\frac{k_n}{2} (V_m - V_{TN})^2 = \frac{k_p}{2} [V_{DD} - V_m + V_{TP}]^2$$

$$V_m = \frac{V_{DD} + V_{TP} + V_{TN} \sqrt{\frac{k_n}{k_p}}}{1 + \sqrt{\frac{k_n}{k_p}}}$$

$V_{IH}$ ,  $P_o$  Sat,  $I_D$  Lin

بنيان الارتفاع

$$\frac{dV_{out}}{dV_{in}} = -1$$

$$V_I = \frac{V_{DD} + V_{TP} + \frac{k_n}{k_p} (V_{TN} + 2V_{out})}{1 + \frac{k_n}{k_p}}$$

$$N_{MOH} = V_{OH} - V_{IH}$$

$$N_{ML} = V_{IL} - V_{OL}$$

\* Symmetric VTC

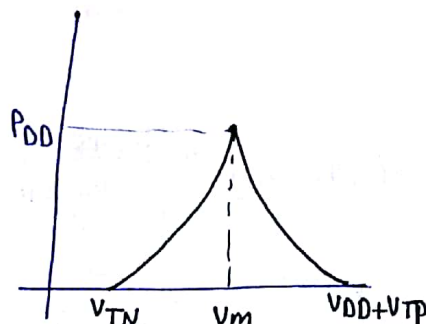
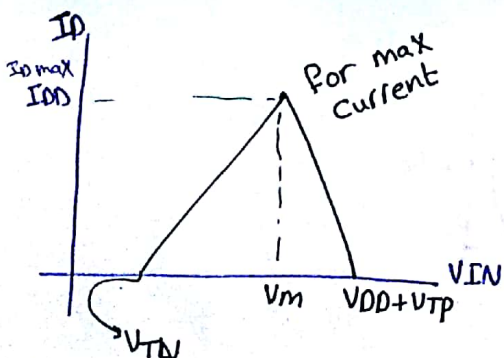
$$V_m - V_{IL} = V_{IH} - V_m$$

$$k_o = k_p$$

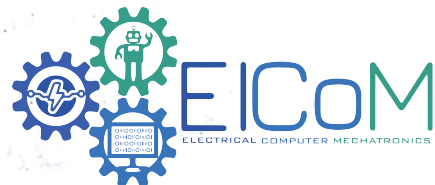
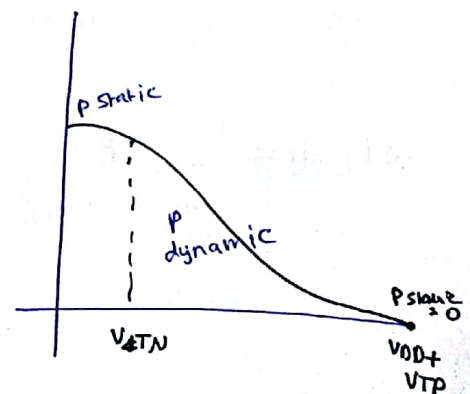
$$\frac{W_P}{L_P} \approx 2.5 \frac{W_N}{L_N}$$

\* Power Dissipation:

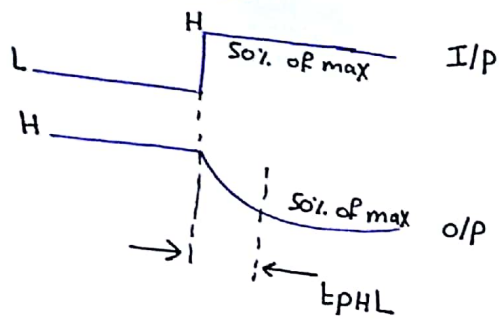
$$\text{Static power} = 0, \text{ dynamic power} = C_L V_{DD}^2$$



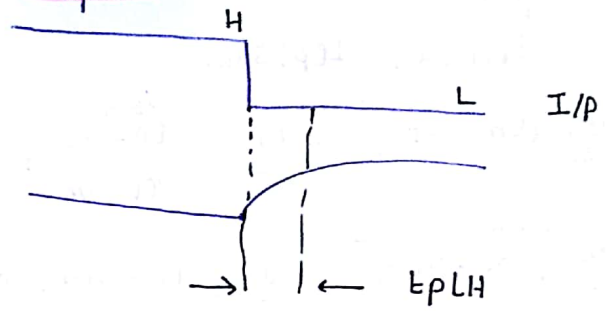
(27)



⇒  $t_{pHL}$



\*  $t_{pLH}$



\*  $k_n = k_p = \mu_n C_{ox} \frac{w_n}{L_n}$   
 - single cap of load -

$$C_{in} = (w_n L_n + w_p L_p) C_{ox}'$$

$$\frac{w_p}{L_p} = 2.5 \frac{w_n}{L_n}$$

\* total cap of load fan-out =  $\frac{C_L}{C_{in}}$

$$\frac{C_L}{k_n} = \frac{F C_{in}}{k} = \frac{F C_{in}}{\mu_n C_{ox}' \frac{w_n}{L_n}}$$

assume  $L_p = L_n \rightarrow w_p = 2.5 w_n$

$$C_{in} = (w_n L_n + 2.5 w_n L_n) C_{ox}$$

$$= 3.5 w_n L_n C_{ox}$$

$$\frac{C_L}{k_n} = \frac{F (3.5 w_n L_n C_{ox})}{C_{ox}' \frac{w_n}{L_n} \mu_n} = \frac{3.5 F L_n^2}{\mu_n} \quad \text{--- (4)}$$

$t_{pHL}$  --- (3)

$$F = \frac{\mu_n}{3.5 L_n^2} \cdot \frac{C_L}{k_n}$$

\*  $F = \mu_n t_p(\max)$

Length  $\rightarrow \frac{3.5 L_n^2}{\left[ \frac{2 V_{TN}}{(V_{DD} - V_{TN})^2} + \frac{1}{V_{DD} - V_{TN}} \ln \left( \frac{1.5 V_{DD} - 2 V_{TN}}{0.5 V_{DD}} \right) \right]}$

$$* t_{pHL} = \left[ \frac{2 V_{TN}}{k_n (V_{DD} - V_{TN})^2} + \frac{L_n}{k_n (V_{DD} - V_{TN})} \ln \left( \frac{1.5 V_{DD} - 2 V_{TN}}{0.5 V_{DD}} \right) \right] C_L$$

$$* t_{pLH} = \left[ \frac{-2 V_{TP}}{k_p (V_{DD} + V_{TP})^2} + \frac{1}{k_p (V_{DD} + V_{TP})} \ln \left( \frac{1.5 V_{DD} + 2 V_{TP}}{0.5 V_{DD}} \right) \right] C_L$$

$$\Rightarrow k_n = k_n' \frac{w_n}{L_{min}} C_{ox}$$

$$\frac{w_n}{L_{min}} = \frac{k_n}{k_n'}$$

$$w_n = L_{min} \frac{k_n}{k_n'}$$

$$w_p = w_n \frac{k_n'}{k_p'}$$

$$\frac{w_p}{w_n} = \frac{k_n'}{k_p'}$$

\* لايبي و max cl , size , length

$$1) t = \dots \text{ (cl)}$$

$$2) C_{in} = (w_L + w_L) C_{ox}$$

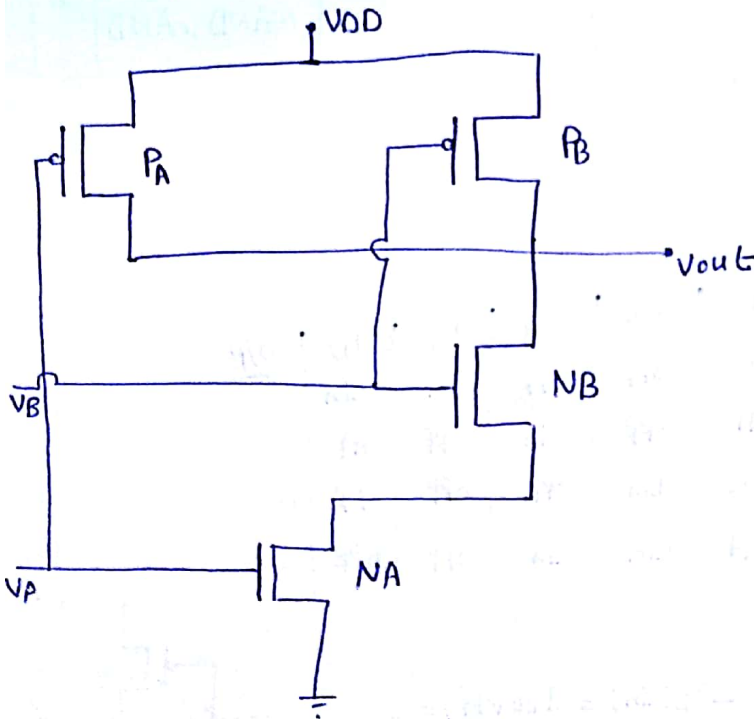
$$3) \frac{w_p}{L_p} = 2.5 \frac{w_n}{L_n}$$

$$* F = \frac{C_L}{C_{in}}$$

نفس التعتيق  
 $V_{TN}$  و  $V_{TP}$  وتأخذ الاقل  
 لايبي عدد ال gate يكون اقل  
 يعني ما يح تستعمل اذا اخذنا الاكبر

Final

Chapter 24:



$V_A$	$V_B$	$N_A$	$N_B$	$P_A$	$P_B$	$O/P$
L	L	off	off	Lin	Lin	H
L	H	off	off	Lin	off	H
H	L	off	off	off	Lin	H
H	H	Lin	Lin	off	off	L

\* ال حالة L, L

$$I_{DPA} + I_{DPB} = I_{DN(A,B)} (off)$$

$$2I_D(Lin) = 0$$

$$I = 0 \rightarrow V_{SD} = 0$$

$$V_{out} = V_{DD} - \cancel{V_{SD}} = V_{DD}$$

\* ال حالة H, L

$$I_{DPB}(Lin) = I_{DN(off)} = 0$$

$$V_{SD} = 0$$

$$V_{out} = V_{DD}$$

⇒

\* For symmetry (AND, NAND)

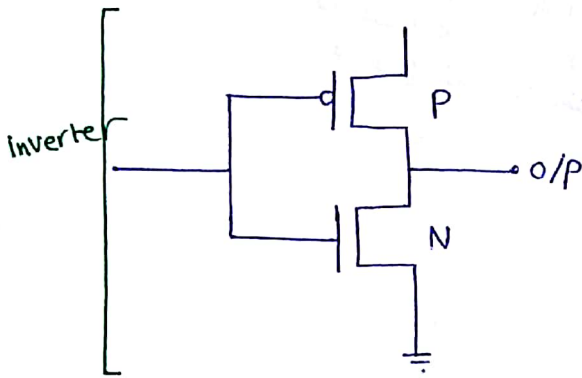
For i I/p CMOS

$$i \frac{w_p}{L_p} = 2.5 \frac{w_n}{L_n}$$

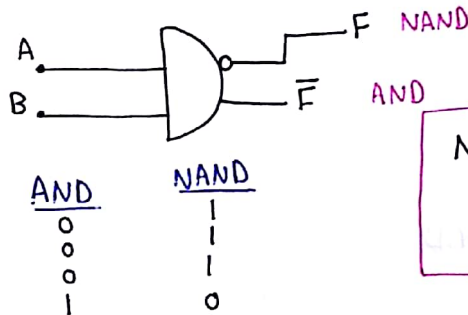
in this case, For 2 I/p CMOS gate

$$2 \frac{w_p}{L_p} = 2.5 \frac{w_n}{L_n}$$

\* لتقريباً من NAND إلى AND نضيف Inverter

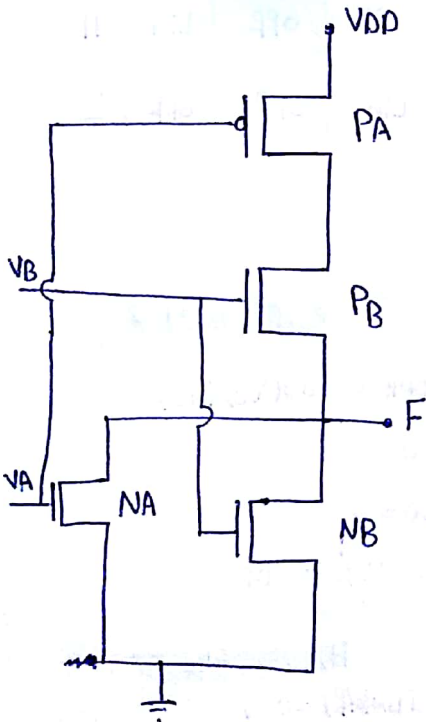


N → pull down ⇒ NAND, AND  
P → pull up



N series, P parallel  
[NAND, AND]

NoR/OR



VA	VB	NA	NB	PA	PB
L	L	off	off	Lin	Lin
L	H	off	Lin	off	off
H	L	Lin	off	off	off
H	H	Lin	Lin	off	off

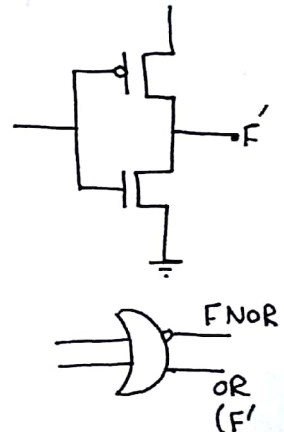
$$2I_D(\text{Lin}) = I_{Dp}(\text{off}) = 0$$

$$V_{oL} = 0 = V_{DS}$$

\* For symmetry (oR, NoR)

$$\frac{w_p}{L_p} = i (2.5) \frac{w_n}{L_n}$$

N parallel, P series  
⇒ [NoR, oR]

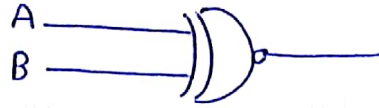




$$= A\bar{B} + B\bar{A}$$

$$A \oplus B$$

$$\text{XOR}$$



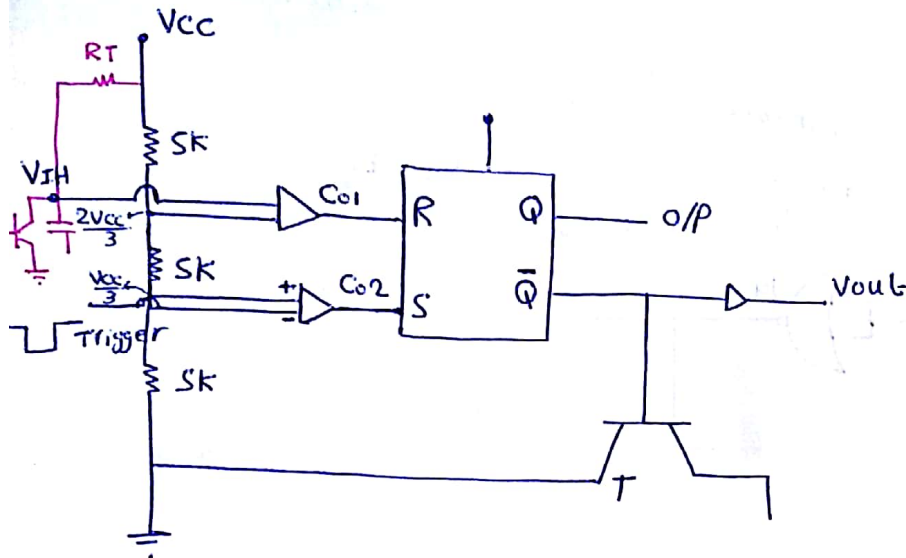
$$\text{XOR}$$

$$\bar{A}\bar{B} + AB$$

$$\overline{A \oplus B}$$

متساوية! مختلفات 0

**\* 555 Timer:**



- ①  $V_{th} \geq \frac{2}{3} V_{cc} \rightarrow C_{01} H \rightarrow \text{Reset } Q=0, \bar{Q}=1$
- Trigger (H)  $V_{th} < \frac{2}{3} V_{cc} \rightarrow C_{01} L \rightarrow \text{Reset } Q=0, \bar{Q}=1, T_{sat} \rightarrow V_c=0$
- Low Trigger  $C_{02}$  لا يتر فقط على  $C_{02}$

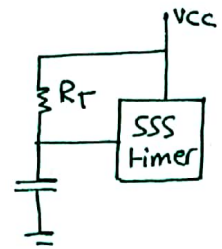
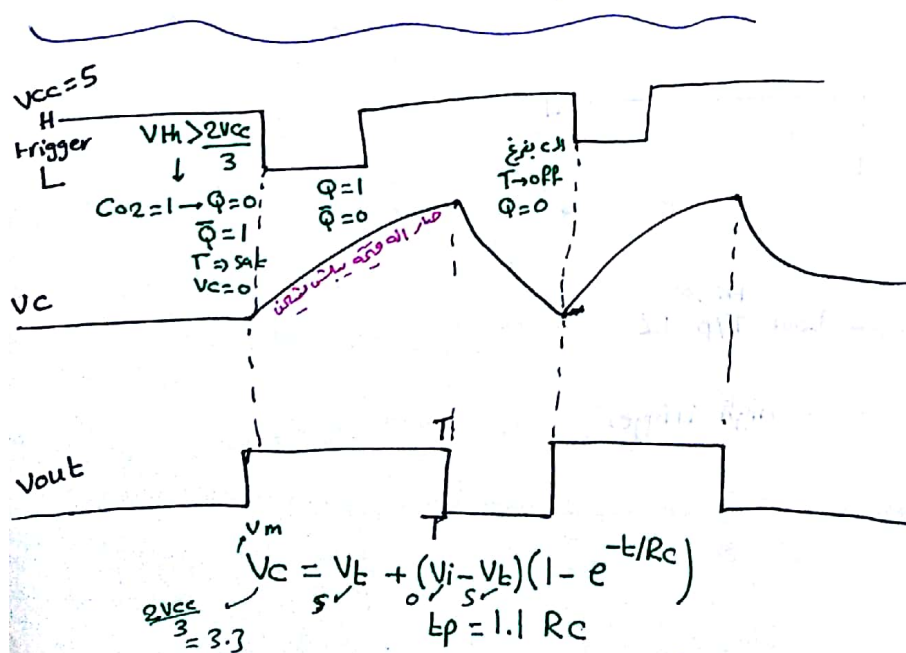
② Trigger L

صوت L على الـ 1 الب تعني  $C_{02}=0$

$$\text{Trigger} > \frac{V_{cc}}{3}$$

Set=1  $Q=1, \bar{Q}=0$   $T_{off}$

$V_c \rightarrow \text{charging}$



لا تشبك

\* اذا ما بعدا نستخدم  $\frac{2V_{cc}}{3}$  يتكلم بناها Controller الـ فيته وداعة نأخذ آخر فيته  $V_{controller} = V_{th} \text{ threshold}$  اذا اقله للـ Controller فيته



⇒ **Multivibrators:**

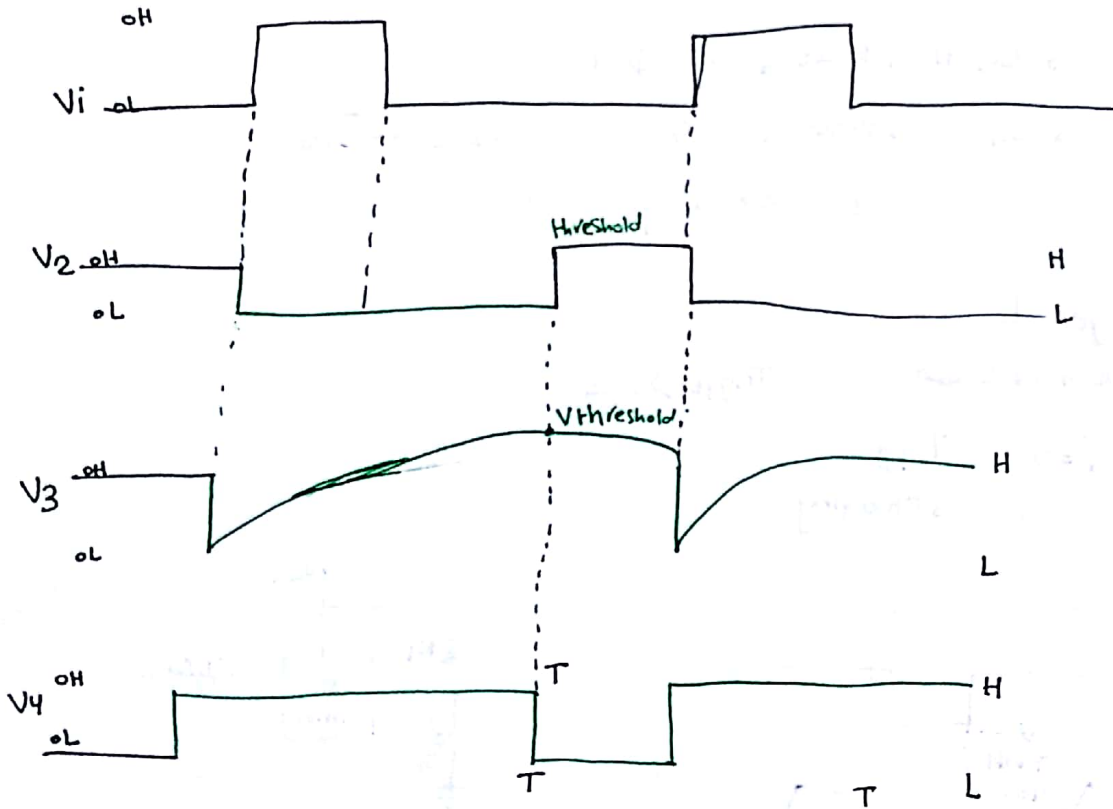
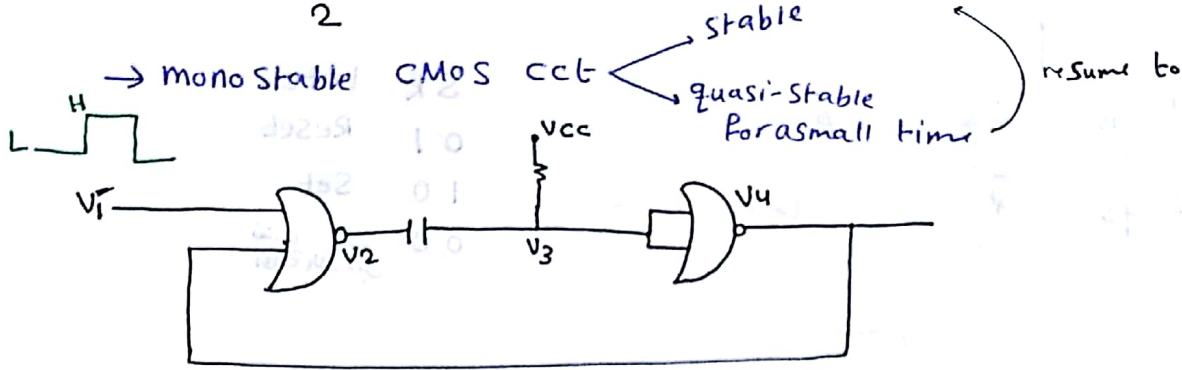
$T = t_2 - t_1$

$T = R_c \ln 2 = 0.7 R_c$

$V_{Th} = V_C = V_i + \frac{(V_f - V_i)}{V_{DD} - 0} (1 - e^{-\frac{t}{R_c C}})$   $T = 0.7 R_c$

\*  $V_{Th} = \frac{V_{DD}}{2}$

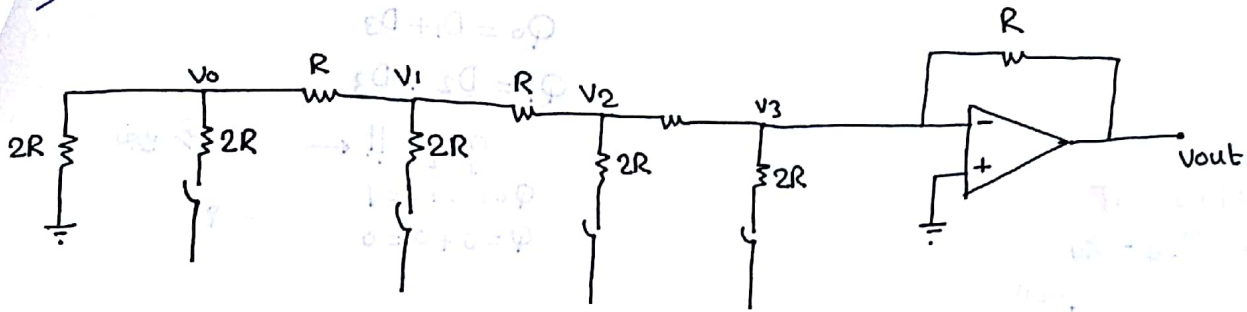
- Concept of
1. non-triggable
  2. re-triggable
  3. Astable
  4. mono-stable
  5. Bi-stable



$V_C = 0$       Low o/p ← Low I/p LL      Trigger

$V_C = \frac{V_{DD}}{2}$       high o/p ← high trigger

## D-A Converter



$$V_{out} = -\frac{V_{ref}}{2} \left( \frac{D_{N-1}}{2^0} + \frac{D_{N-2}}{2} + \dots + \frac{D_1}{2^{N-2}} + \frac{D_0}{2^{N-1}} \right)$$

$$V_{out} = -\frac{n}{2^N} V_{ref}$$

$$V_{ref} = \frac{\# \text{ of Levels}}{\# \text{ of Counts}} \cdot \frac{V_{out}}{V_{o \max}}$$

$$Res = \frac{V_{ref}}{2^N - 1}$$

$$Acc = \frac{Res}{V_{ref}} = \frac{1}{2^N - 1}$$

## A-D Converter

$$Res = \frac{V_{ref}}{N+1}$$

$$Acc = \frac{Res}{V_{ref}}$$

إذا المخرج صفر وفيها R في المقام = عدد R

إذا المخرج دون حركة، فقط عدد Comp في المقام +1 عدد Comp

عدد D التي عندهم 1 ارضعاني

$$V_{ref, m} = \frac{m}{n+1} V_{ref} < V < \frac{m+1}{n+1} V_{ref}$$

حسب

لا آلتب مثلا الرقم وعندي 8-3 encoder (101)

$$Q_0 = D_1 + D_3 + D_5 + D_7 = X + X + 1 + 0 = 1$$

$$Q_1 = D_2 + D_3 + D_6 + D_7 = X + X + 0 + 0 = 0$$

$$Q_2 = D_4 + D_5 + D_6 + D_7 = X + 1 + 0 + 0 = 1$$

$$= 101$$

تسمية

dig o/p of Comp = dig I/p of encoder

= binary # prior to encoder

حسب ال 8-3 encoder (يكون اما 8 ادا 4)

dig encoder o/p → يكون 2 ادا 3

00000001 = dig o/p ← مثل EX الرقم انه لملنا قيمة m وطلعة مثلا 1

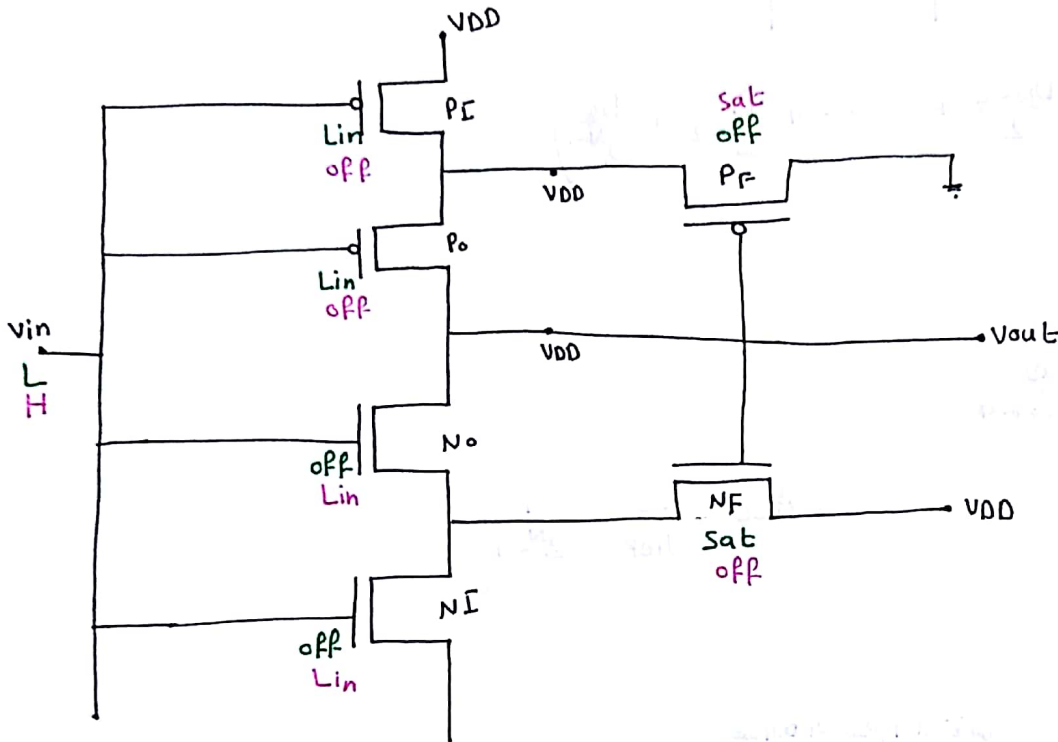
00001111

لو مثلا 4

N=8 و

## 26. CMOS ST

$$\text{Hysteresis} = V_{ID} - V_{IH}$$



$$V_{OH} = V_{DD}$$

$$V_{OL} = 0 \rightarrow I = 0 \rightarrow V_{SD} = 0$$

$$* V_{IL} = V_{IH} = \frac{\sqrt{\frac{K_{PI}}{K_{PF}}} (V_{DD} + V_{TP})}{1 + \sqrt{\frac{K_{PI}}{K_{PF}}}}$$

$$I_{D,PI}(\text{sat}) = I_{D,PF}(\text{sat})$$

$$\frac{K_{PI}}{2} [(V_{SG,PI} + V_{TP})^2] = \frac{K_{PF}}{2} [(V_{SG,PF} + V_{TP})^2]$$

$V_{DD} - V_{in}$

$$V_m = \frac{V_{DD}}{2}$$

$$* V_{IH} = V_{ID} = \frac{V_{DD} + \sqrt{\frac{K_{NI}}{K_{NF}}} V_{TN}}{1 + \sqrt{\frac{K_{NI}}{K_{NF}}}}$$

$$I_{D,NI}(\text{sat}) = I_{D,NF}(\text{sat})$$

