

تقدم لجنة EiCoM الاكاديمية

دفتر لمادة:

# الالكترونيات 2

جزيل الشكر للطالب:

# قتيبة الكعابنة



1)  $R_E$  in C.E

- is used to stabilize Q-pt against  $\beta$ -Variation [advantages]
- Reduce  $A_V$  and  $A_I$  [disadvantages]
- Increase  $R_i$  [advantages]
- Stabilize  $A_V$  and  $A_I$  against  $\beta$ -Variation [advantages]

2) When  $C_E$  is connected

- 1)  $D_C$ -values unchanged
- 2)  $A_V, A_I$ , increase
- 3)  $R_i$  decrease

3) Characteristics of C.E

- 1)  $A_V > 1$
- 2)  $A_I > 1$
- 3)  $\phi$ : phase shift  $180^\circ$
- 4)  $R_i$ : moderate

$R_o$ : moderate to high

4) Characteristics of C.C [Emitter follower]

- 1)  $A_V < 1$
- 2) high current gain  $A_I > 1$
- 3)  $R_i$ : high
- 4)  $R_o$ : low

5)  $\phi$ : zero

\* it used 1) power Amp

2) Buffer [minimize Loading effect]

or to provide no Loading effect

## 5) Characteristics of E.B [Current-Follower]

1) High Voltage gain  $A_V > 1$

2) Low Current gain  $A_I < 1$

3)  $R_i$ : Low, 4)  $R_o$ : High

$\phi$ : Zero

## 6) ~~B~~ Darlington

1)  $A_I$ : very high  $\approx \beta^2$

2)  $R_i$ : high

⇒ Cascade: used as wide band Amp

# 1) Common Source

## (i) Basic

-  $R_{in}$

$$R_{in} = \infty$$

$$R_{in} = R_1 // R_2 = R_g$$

$R_i$  seen by the voltage source  $= R_{in} + R_s$

-  $R_{out}$

$$R_o = R_D // R_D$$

## (ii) with $R_s$

$R_s$  is used to stabilize  $Q_{pt}$  against  $K_n$  Variation

$$R_{in} = \infty$$

$$R_{in} = R_1 // R_2$$

$$R_i \text{ seen} \dots = R_s + R_{in}$$

$$R_o = R_D$$

## (iii) with bypass cap ( $C_b$ )

$$R_{in} = R_1 // R_2$$

$$R_{in} = \infty$$

$$R_i \text{ seen} \dots = R_s + R_{in}$$

$$R_o = R_D$$

\* زيادة  $C_b$  يقوم بزيادة  $A_v$  من الحالة (ii)

\* خواص Common Source

(1)  $A_v$  أكبر من 1

(2) زاوية الطور  $180^\circ$

(3)  $R_o = R_D$  متوسطه

(4)  $R_{in} = R_{in}$

## \* 2) Common Drain [Source - Follower]

1)  $A_V < 1$  لا يتكبر  
Voltage Amp

2)  $R_O$  Low  $\Rightarrow R_O = \frac{1}{g_m} \parallel r_o \parallel R_S$

3)  $R_{in} = R_g$

4)  $\phi = 0$

## \* 3) Common Gate

1)  $A_V > 1$

2)  $\phi = 0$

3)  $R_{in} = R_S \parallel R_{ins} = R_S \parallel \frac{1}{g_m}$  Low

4)  $R_O = R_D$  Moderate to high ~~low to high~~

\*

Cascode: used high freq  
[wide band Amp]

$$A_V \text{ Cascode} = A_V \text{ CS}$$

\*

$$I_D = k_n [V_{GS} - V_{TN}]^2$$

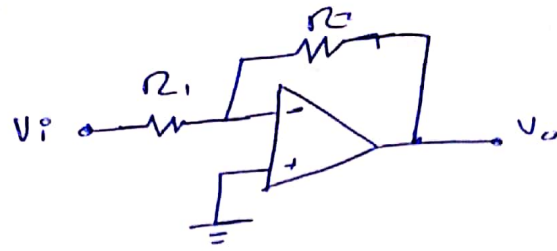
$$V_{GS} = V_{TN} \pm \sqrt{\frac{I_D}{k_n}}$$

$$g_m = 2\sqrt{k_n I_D}$$

$$r_o = \frac{1}{\lambda I_D}$$

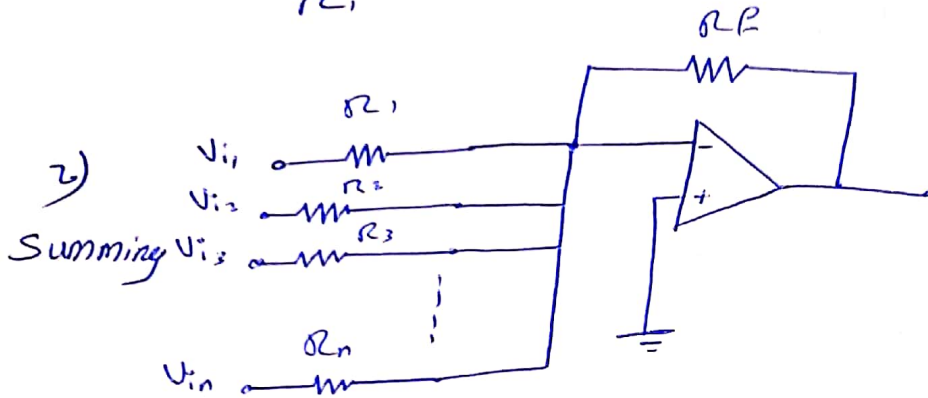
# \* Linear

## 1) Inverting



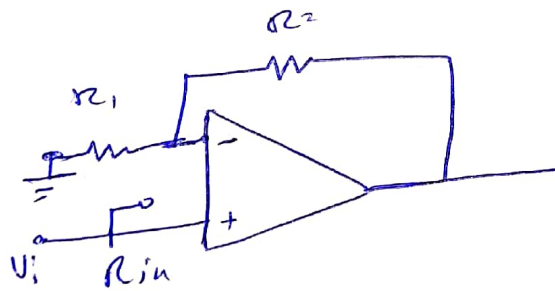
$$R_{in} = R_1$$

$$AV = -\frac{R_2}{R_1}$$



$$V_o = \left[ -\frac{R_f}{R_1} V_{i_1} + \frac{R_f}{R_2} V_{i_2} \dots - \frac{R_f}{R_n} V_{i_n} \right]$$

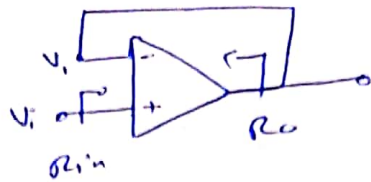
## 3) Non Inverting



$$AV = \left[ 1 + \frac{R_2}{R_1} \right] = \frac{V_o}{V_i}$$

$$R_{in} = \infty$$

#### 4) Voltage-Follower "Buffer"

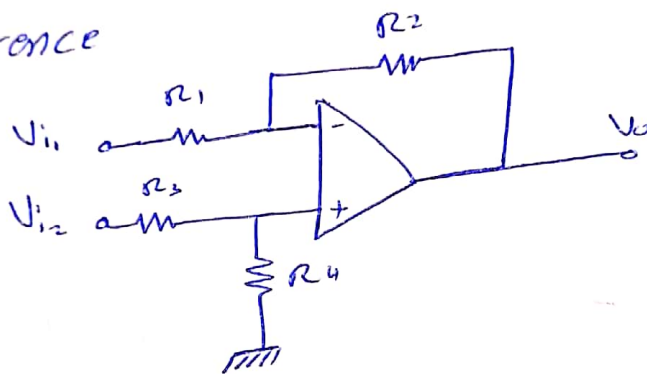


$$[A_v = 1, R_{in} = \infty, R_o = 0, \phi = 0]$$

Characteristics of Ideal Voltage-Follower

\* used to minimize Loading effect

#### 5) Difference



$$V_o = \left[ \left( 1 + \frac{R_2}{R_1} \right) \left( \frac{R_4}{R_3 + R_4} \right) V_{i2} - \frac{R_2}{R_1} V_{i1} \right]$$

if  $\frac{R_4}{R_3} = \frac{R_2}{R_1}$

$$A_d = \frac{R_4}{R_3} = \frac{R_2}{R_1}$$

$$R_{id} = R_1 + R_3$$

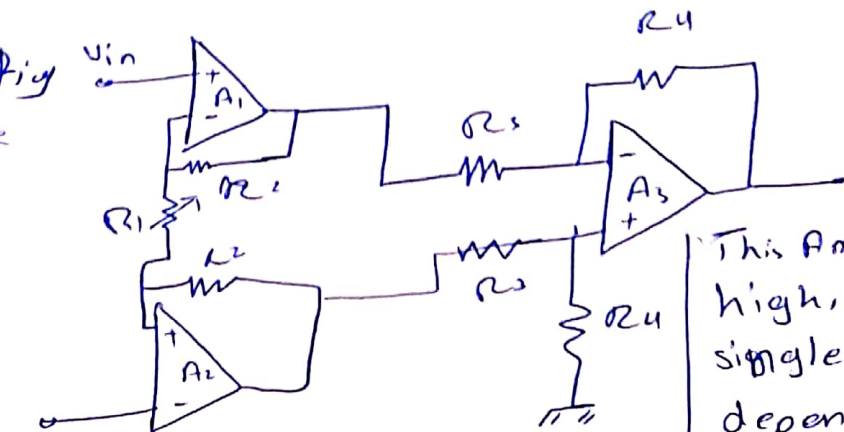
#### 6) Instrumentation

1) \$A\_1, A\_2 \Rightarrow\$ Non inverting  
\$A\_3 \Rightarrow\$ Difference

2) \$R\_{in1} = \infty, R\_{in2} = \infty\$  
\$R\_{id} = \infty\$

3)  $A_d = \frac{R_4}{R_3} \left[ 1 + \frac{2R_2}{R_1} \right]$

$\frac{A_{min}}{\frac{R_4}{R_3}} > 1$   
For design

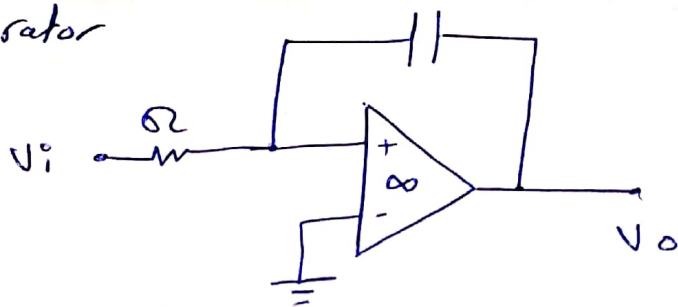


To change \$A\_d\$ we change \$R\_1\$ only

This Amp achieves high, adjustable, single-element, dependant gain and very high input- $R$

using proper values

### 7) Integrator

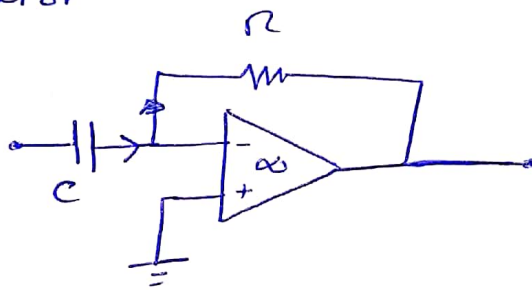


$$V_o = -\frac{1}{RC} \int v_i dt$$

$V_i \Rightarrow$  Square

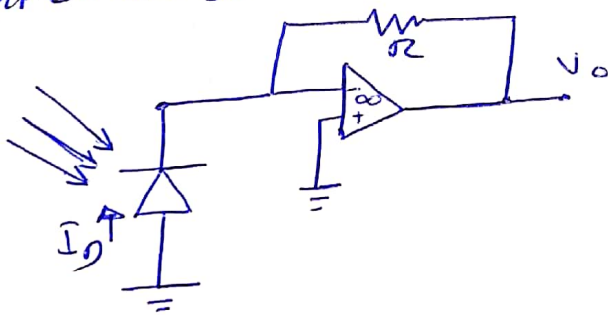
$V_o \Rightarrow$  Triangular

### 8) Differentiator



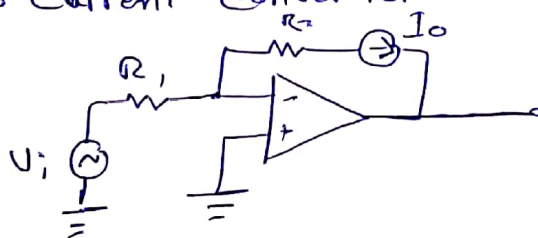
$$V_o = -RC \frac{dv_i}{dt}$$

### 9) Current to Voltage converter



$$V_o = -I_D R$$

### 10) Voltage to Current converter

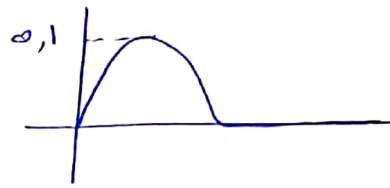
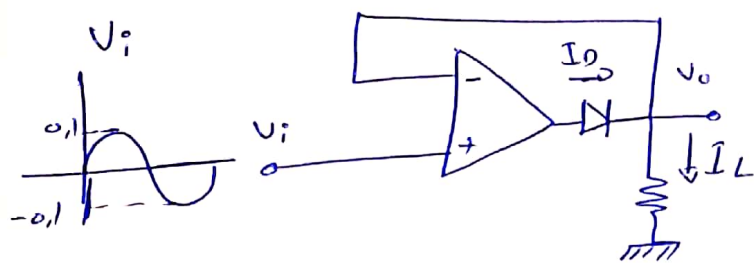


$$I_o = -\frac{V_i}{R_1}$$



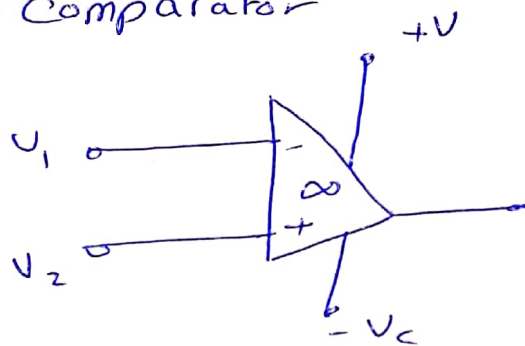
# \* Non Linear

## 1) precision Half-wave Rectifier



$$V_{o \text{ avg}} = \frac{V_{ip}}{\pi}$$

## 2) Voltage - Comparator



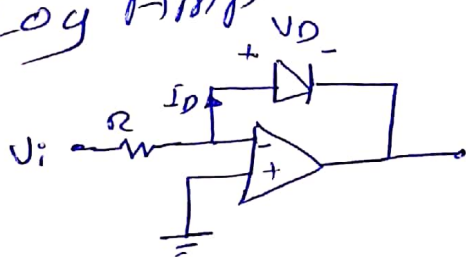
used in open loop mode  
[no connection between \$V\_o\$ and (-) terminal]

1)  $V_2 > V_1$   
 $V_o = +V_c$

2)  $V_2 < V_1$   
 $V_o = -V_c$

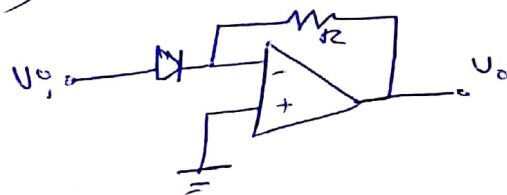
\* IF  $V_{ref} = 0$   
Then O/P is symmetrical square-wave and the circuit is called [Zero-crossing detector]

## 3) Log AMP



$$V_o = -nV_T \ln \frac{V_i}{I_s R_s}$$

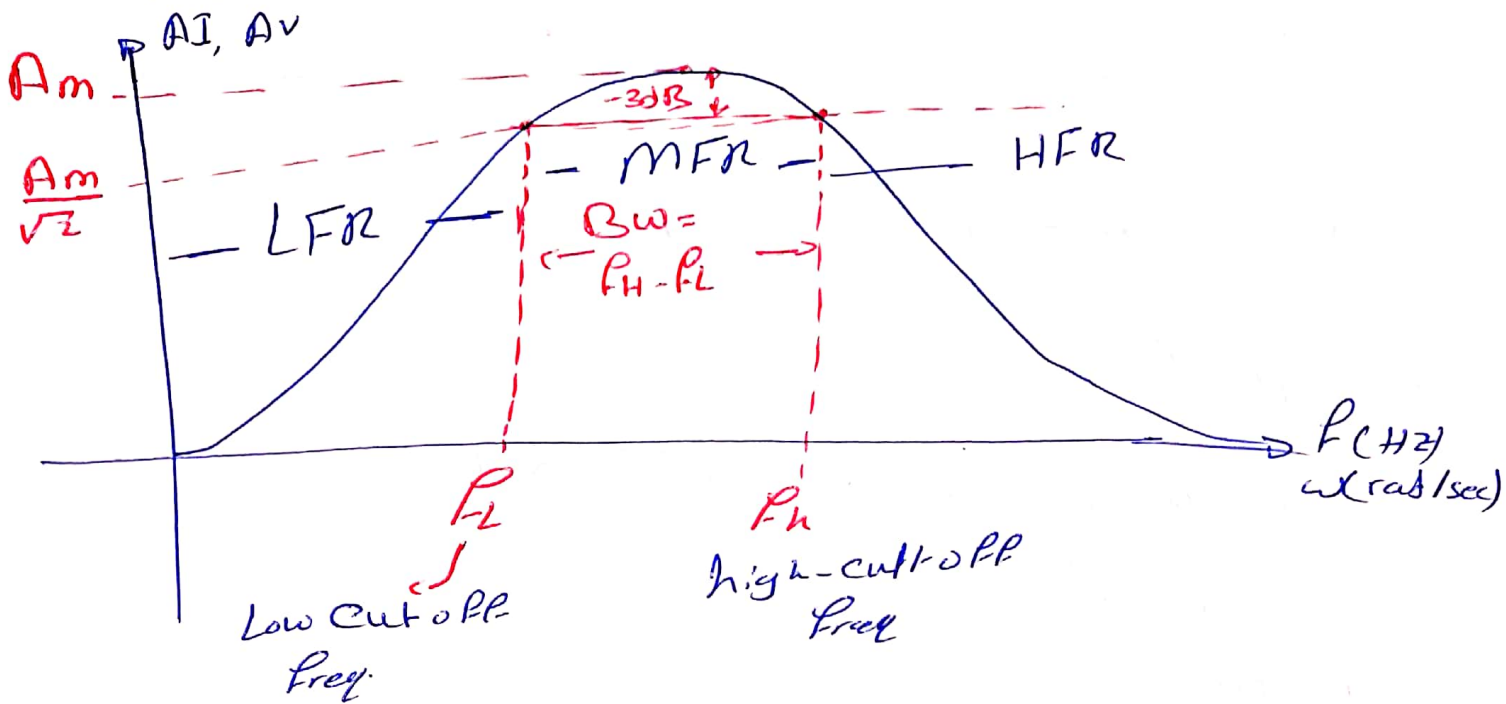
## 4) Antilog or Exponential



$$V_o = -I_s R e^{\frac{V_i}{nV_T}}$$

# \* Frequency Response

$$A_V(\text{dB}) = 20 \log A_V = 20 \log \frac{V_o}{V_s}$$



## 1) Low Freq - Regn

- This Regn extends from  $[0 - f_L]$
- $f_L, A_V \uparrow$  كالتالي
- $f_L, A_V$  (الفرق بين  $f_L, A_V$ )
- $C_1, C_2, C_E$  و  $f_L$

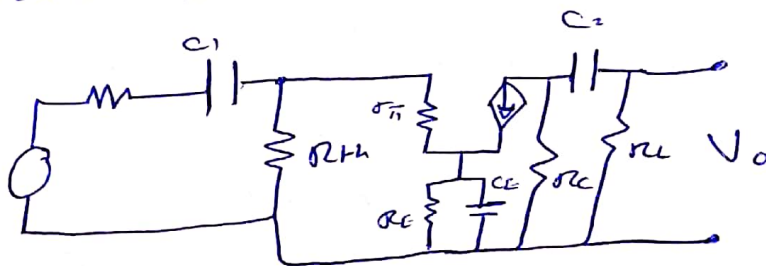
Av يزداد مع f  
 لأن Cap في input لها impedance

$$f_L, X_C \downarrow, V_B \uparrow, V_C \uparrow, V_o \uparrow, A_V \uparrow$$

$$X_C \approx \frac{1}{2\pi f C}$$

## \* $C_{\pi}$ and $C_{\mu} \Rightarrow \infty$

$$X_{C_{\pi}} = \infty = X_{C_{\mu}}$$



## 2) Medium freq Regn

- This Regn extend from  $[f_L - f_H]$
- This is a useful Regn of Amp operation
- In this Regn all coupling and bypass  $\Rightarrow$  short ckt  
 $[C_1, C_2]$   $(C_E)$
- $C_{\pi}, C_M \Rightarrow$  open ckt,  $X_M = X_{C_{\pi}} = \infty$

## 3) High freq Regn

- This Regn extend from  $[f_H - \infty]$
- زيادة  $f$  يؤدي إلى تقليل  $A_V$
- $C_1, C_2$  and  $C_E \Rightarrow$  short ckt
- $C_{\pi}$  and  $C_M \Rightarrow$  ~~ظهور~~ <sup>أثر</sup> ~~ظهور~~ <sup>في</sup> هذه المنطقة  
\* ما الهموم وجوده، فيزيائياً ورسماً تظهر  
بسبب التركيب الفيزيائي لـ BJT
- $C_{\pi} \therefore$  B-E Jn [F.w biased Jn]
- $C_M \therefore$  Reversed biased Jn

\* Miller  $\therefore$  نظرية تقوم بتوزيع  $C_M$    
  $L_{hearm}$

\*  $f_T, X_C \downarrow, (R_L // X_{C_{m2}}) \downarrow, A_V \downarrow$

\*  $C_L \therefore$  is connected in parallel with  $R_L$   
 $L_C$  control  $f_H$  and make it not depend  
on  $C_M, C_{\pi}$